### Feedback control systems

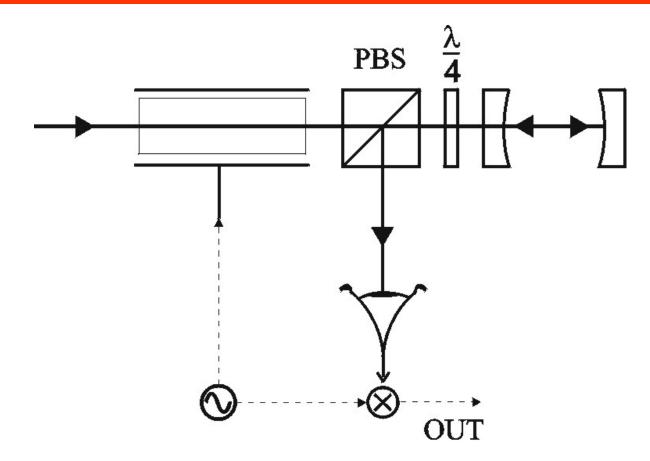
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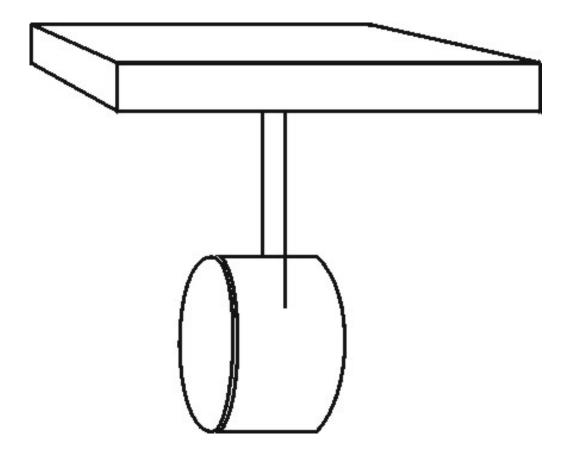
## Outline

- Why feedback?
- What is feedback?
- How does feedback work?
- Benefits of feedback
- Feedback example
- Costs of feedback
- Glimpse of overall feedback in LIGO

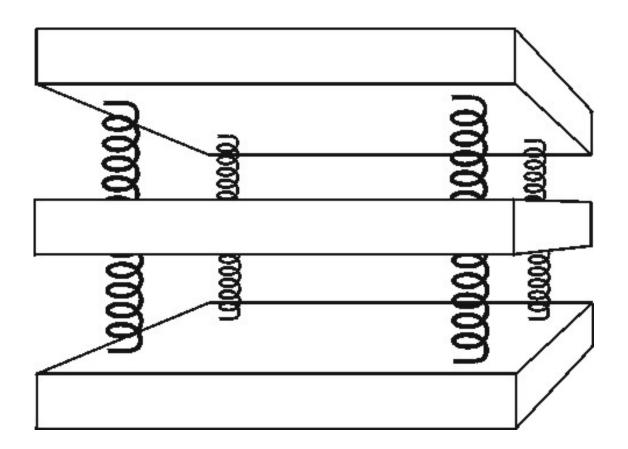
# How can we match $\lambda$ to the length of a resonant cavity?



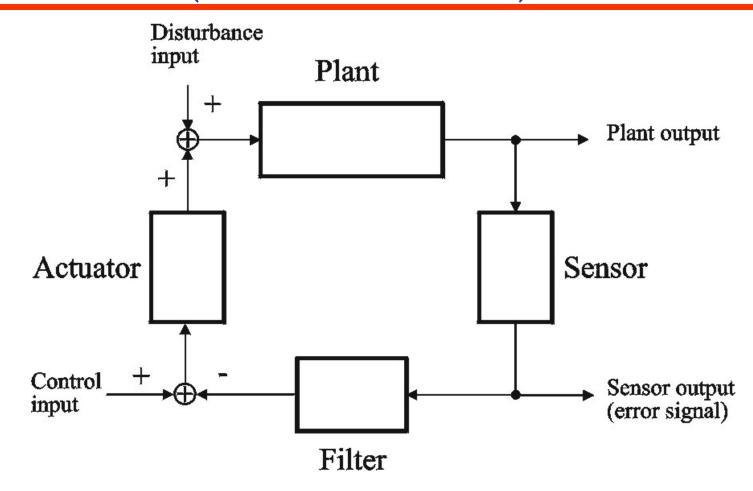
### How can we modify the response of a test mass suspension?



How can we improve vibration isolation?



### A feedback control system (a.k.a. "servo")



### Parts of a servo

- *Plant*: The pre-existing system that you want to control or modify.
- *Sensor*: Generates an (electronic) signal proportional to the plant's output.
- *Actuator*: Acts on the plant to change its output in the desired way.
- *Compensation filter*: (more on this later)

Feedback can hold the plant near a chosen operating point

- Control input is zero. But disturbance inputs cause the plant output to vary.
- Sensor measures the fluctuating plant output.
- Actuator applies a force proportional to the negative of the plant output, thus holding the plant near the chosen operating point.

*Feedback reduces sensitivity to disturbance inputs.* 

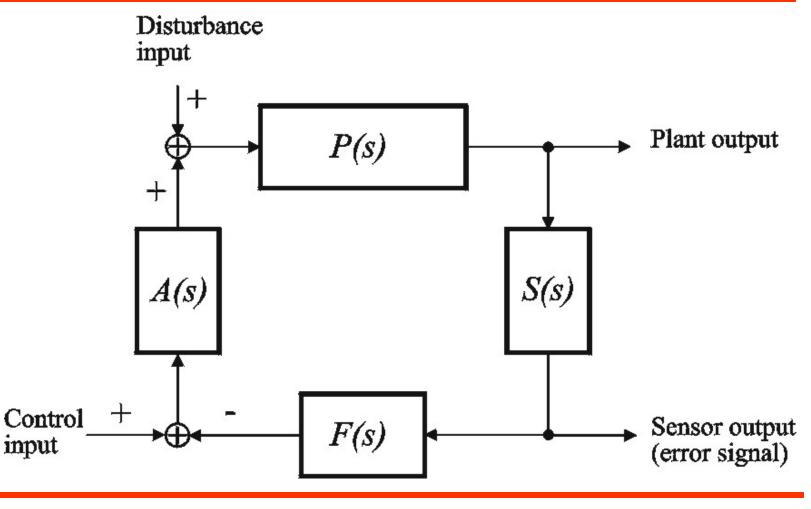
Feedback can modify the dynamics of the plant

Plant responds to control inputs or to disturbance inputs.

Sensor measures the response, which is modified by the compensation filter.

Actuator applies a force that combines with inputs, so that the response of the plant is different than the response to external inputs alone.

### Dynamics of a servo



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Loop Transfer Function (a.k.a. loop gain)

The *loop transfer function* of a feedback control system is given by

$$G(f) \equiv P(f)S(f)F(f)A(f).$$

*G*(*f*) determines the behavior of the servo, how it modifies the performance of the plant, and also the stability of the system.

Benefits of feedback: Closed loop transfer function

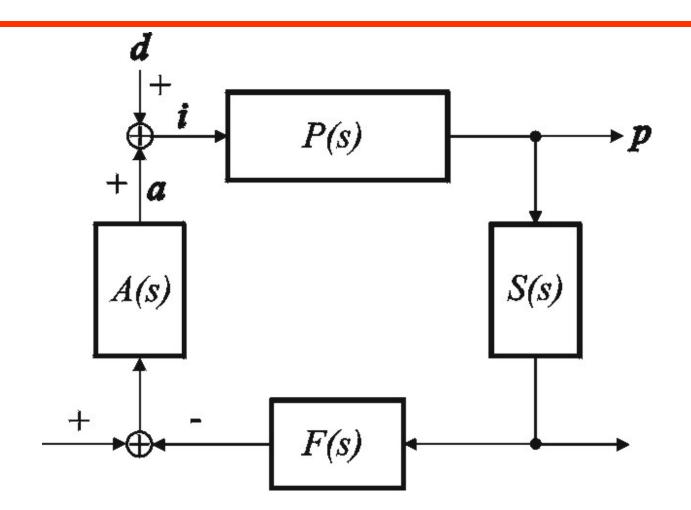
Let *H*(*f*) be a transfer function between any two points when the loop *is not* closed.

Let  $H_{cl}(f)$  be the same transfer function when the loop *is* closed.

Then

$$H_{cl}(f) = \frac{H(f)}{1 + G(f)}.$$

### Signals in servo



# Derivation of closed loop transfer function

$$i \equiv d + a.$$
  

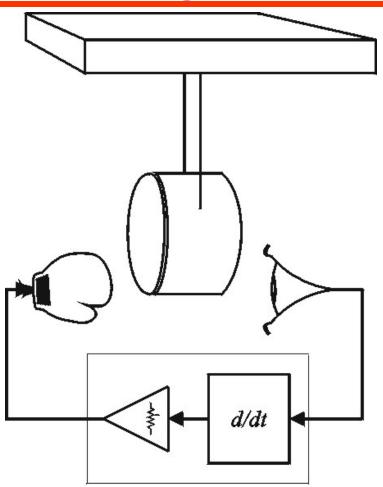
$$a = -iPSFA \equiv -iG.$$
  
Thus  $i = d - iG$ , or  $i = \frac{d}{1+G}.$   
So, for ex.,  $P_{cl} \equiv \frac{p}{d} = \frac{P}{1+G}$ 

### Benefits of feedback

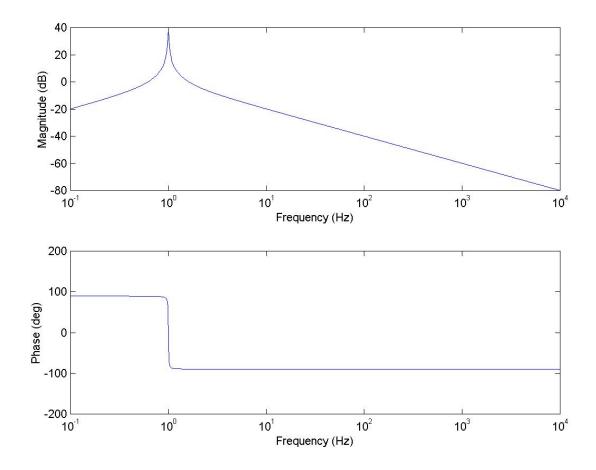
Servo does a lot at frequencies where 1+*G* is large, a little where 1+*G* is of order unity, and almost nothing where *G*<<1.

This is one reason why we say that the benefits of feedback are all encoded in the loop transfer function *G*.

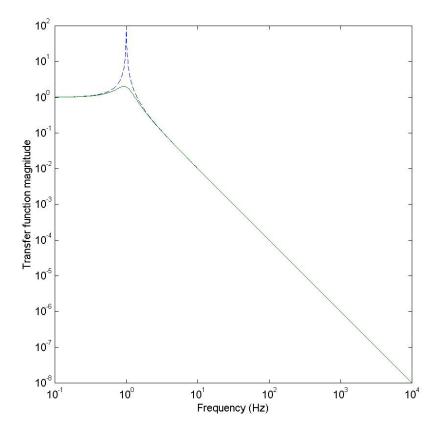
# Example: active damping of pendulum



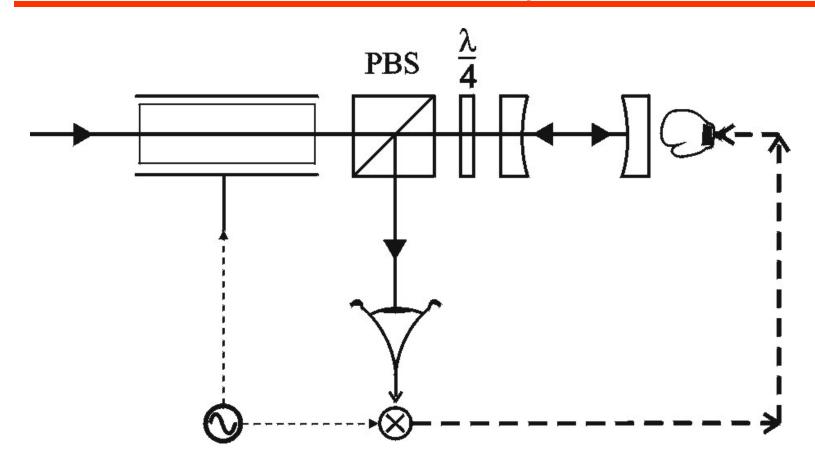
# Active damping: loop transfer function



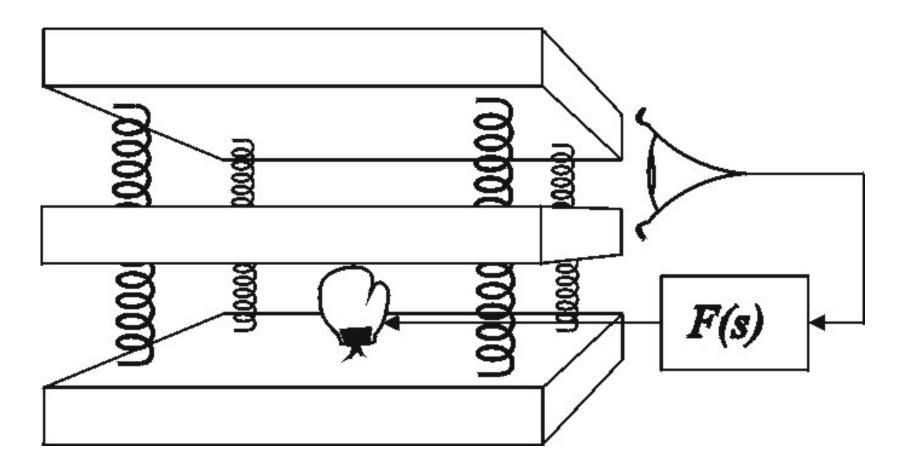
# Active damping: Open loop, closed loop transfer functions



# Example: Resonant cavity lock



## Example: Active vibration isolation



### Costs of feedback

- Some cost: Feedback control systems need extra parts, and those need to be carefully designed.
- Biggest "cost": To ensure that the servo will be *stable* when the loop is closed.
- Frequency dependence of the loop transfer function *G* is critical. This is the main role of the compensation filter *F*.

This is a very rich subject!

# Stability and causality

Recall:

$$H_{cl}(f) = \frac{H(f)}{1 + G(f)}.$$

What happens if, for some f, G(f) = -1?

Closed loop response diverges!

Why not just avoid this, e.g. by making *G* large for all *f*?

- Causality requires that response of physical systems can't keep fixed magnitude and phase to arbitrarily high *f*.
  - Speed of light

In mechanical systems, the speed of sound is the real limit!

# Ensuring stability

- Generically, at high frequencies we accumulate large phase lags.
- When  $\phi$  = -180 deg, we've picked up an unwanted change of sign.
- The standard way to deal with this is by ensuring that the magnitude of the loop transfer function *G* is small for all *f* above that point.
- Ensuring stability requires careful design of the compensation filter *F*.

# Limits to filter design

Almost always, our first guess at the filter that we'd like is impossible to realize.

For example, I'd love to have a filter that has strongly decreasing gain with frequency, but has constant phase.

A theorem of complex analysis forbids the separate specification of |G(f)| and  $\varphi(f)$ . Specifying one uniquely specifies the other.

$$|G(f)| \propto f^{-N} \to \varphi(f) = -N * 90^{\circ}$$

# Stability tests

Feedback designers most often study the Bode plot of G(f), and have developed rules of thumb for estimating when a loop will be stable. For example, if the phase of G only departs from 0 by more than  $\pi$  at frequencies at which the magnitude of G is less than 1, the loop is usually stable.

*N.B.*: <u>There is no rigorous stability test that can</u> <u>always be applied by study of the Bode plot.</u>

# Rigorous stability tests

- The Nyquist diagram, in which one plots *G*(*f*) in the complex plane.
  If there are no encirclements of (-1,0), the loop is stable.
- The root locus method. If all of the roots of the closed loop response lie in the left half-plane, the system is stable.

State space methods, a.k.a. "modern control theory"

For complicated systems, it is often best to abandon frequency domain methods, and work directly with a model of the equations of motion of the system.

A well-developed version of this is called *state space control*. There are good books on this subject ...

### How Does it All Hang Together?

