

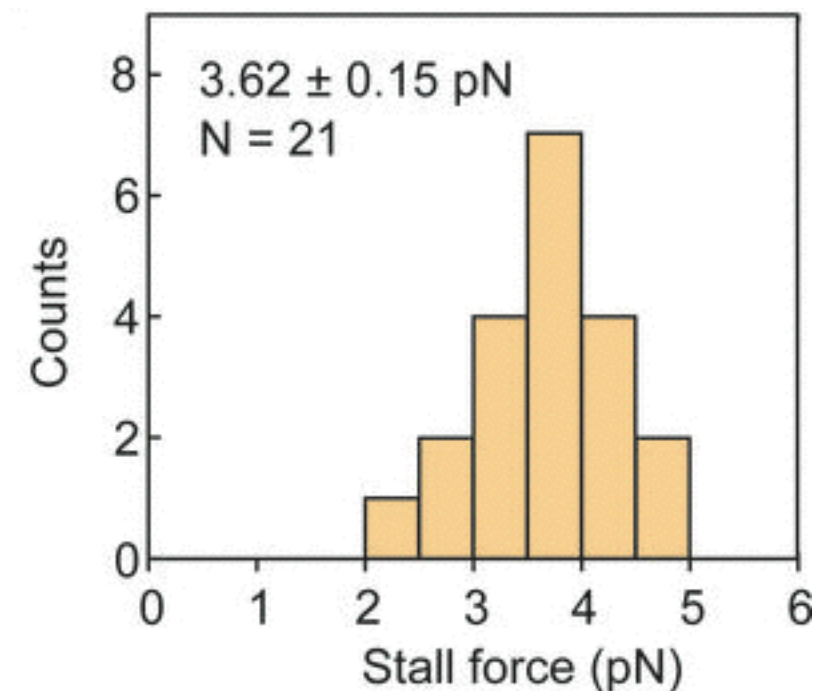
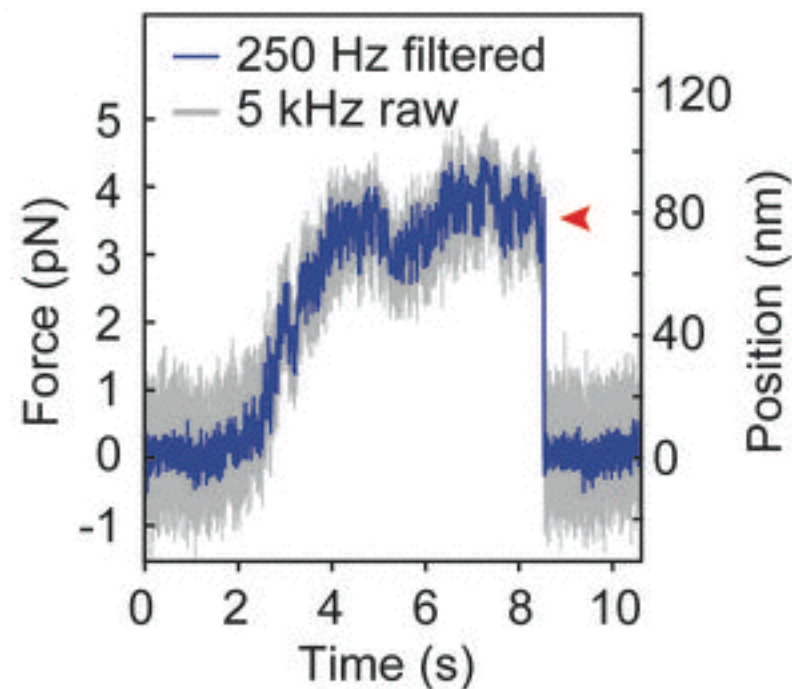
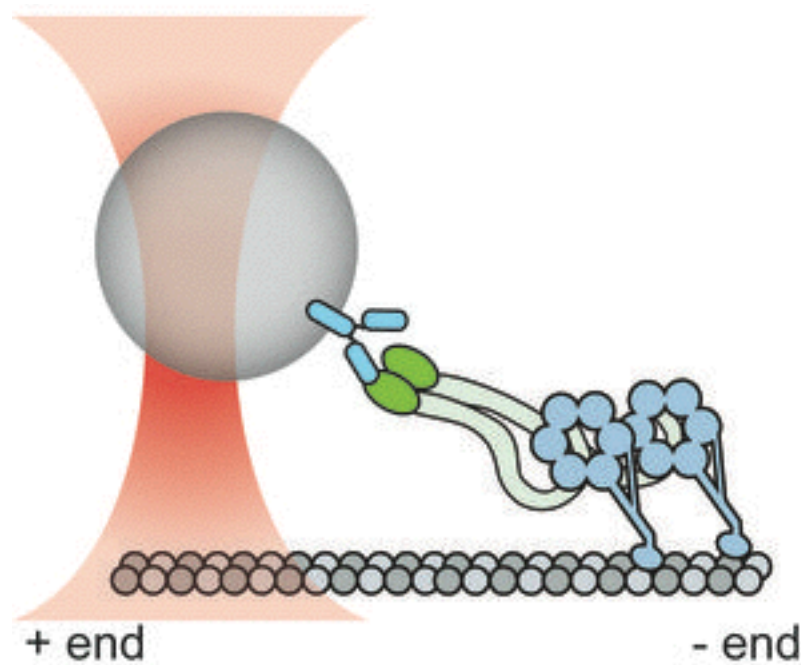
Additivity of Maximum Force Generated by Multiple Filaments or Motors

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Sciences, University of Mumbai**

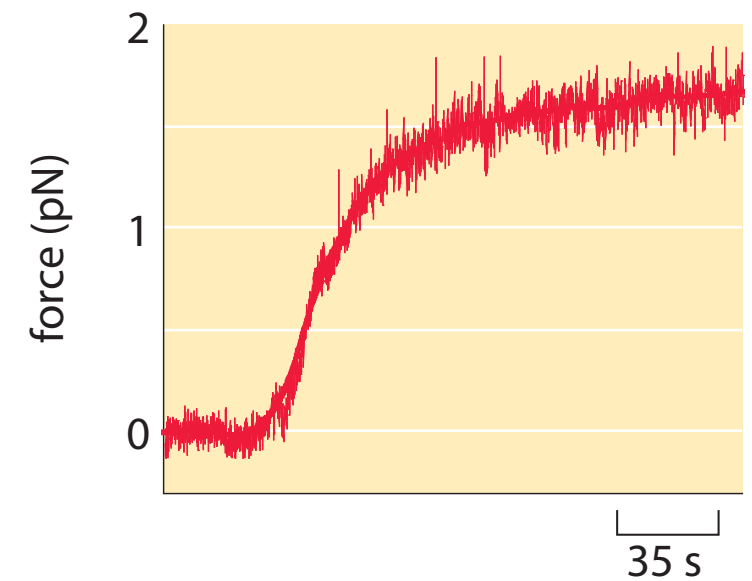
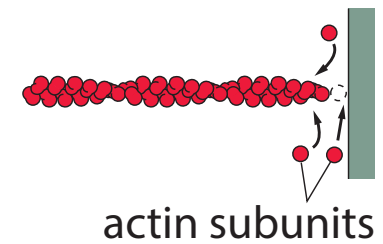
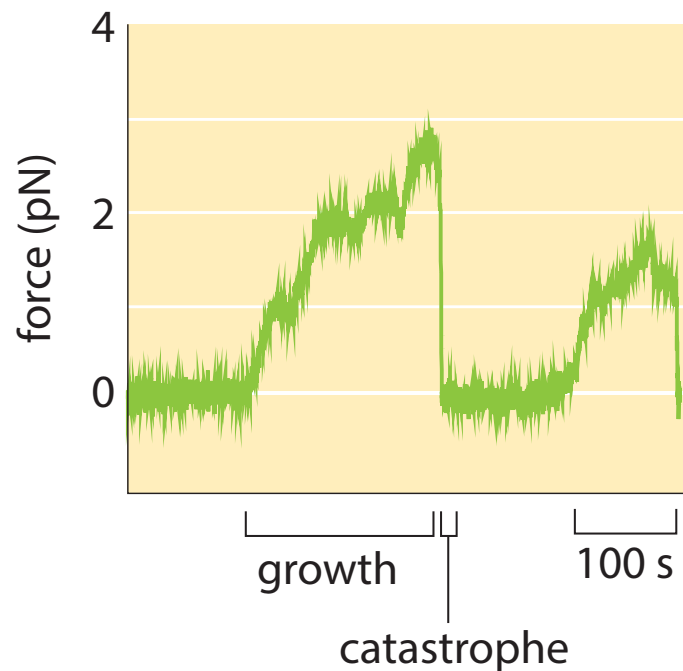
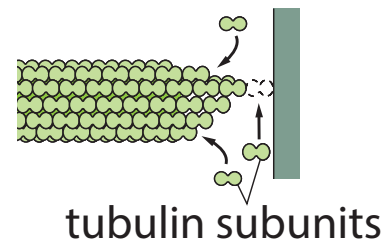
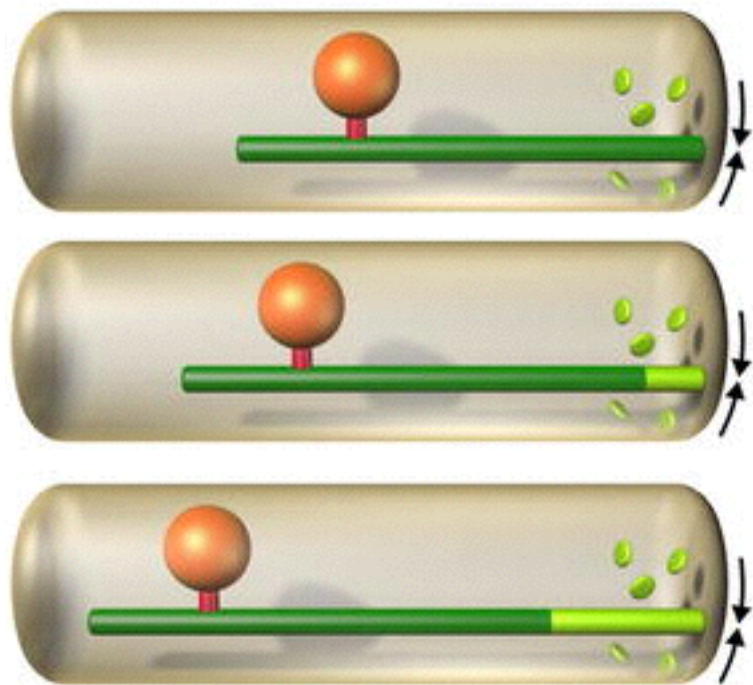
Force generation by Molecular motors

Most forms of movement in the living world are powered by tiny protein machines.



Force generation by Bio-filaments

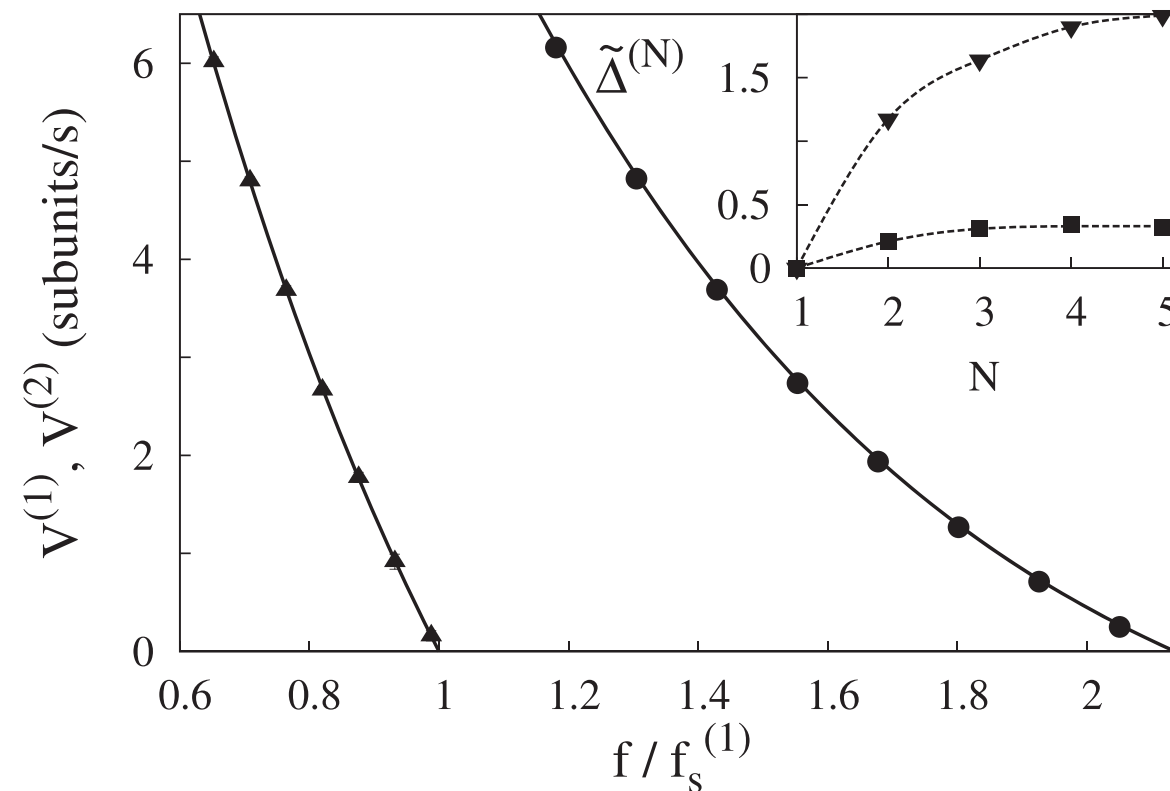
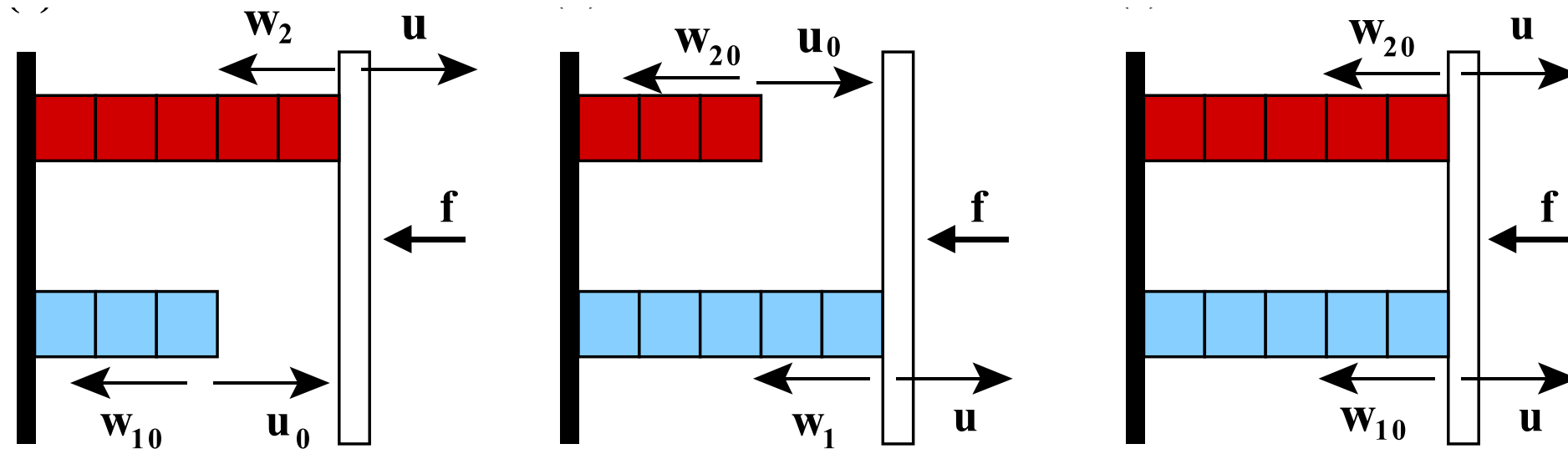
Simplest Nano-machine, utilize chemical energy of polymerization to generate significant amount of force



Iva Tolic, 2008, EBJ

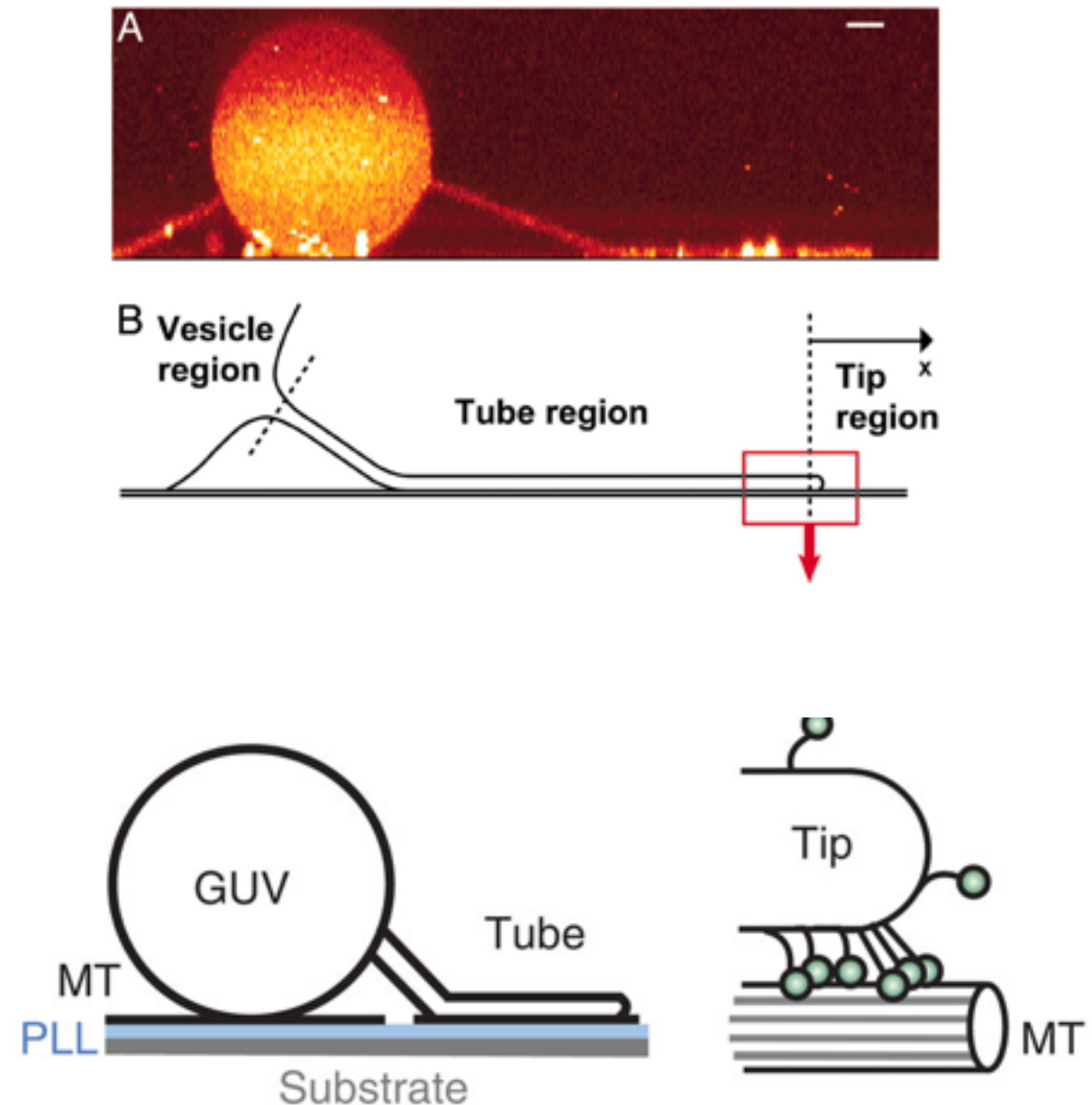
How stall force scales with number of filaments/motors?

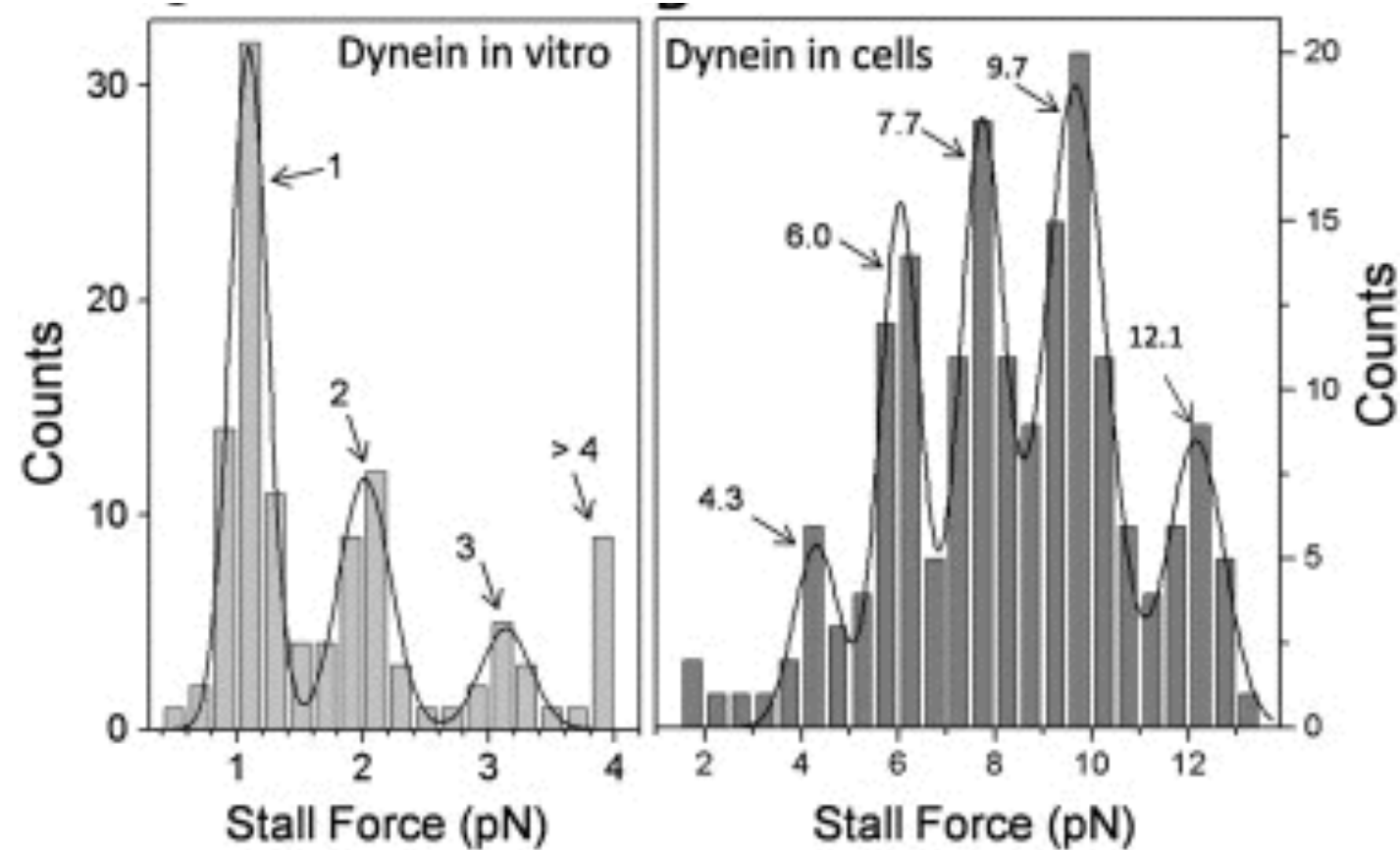
Stall force generated by multiple filament



Cooperative force generation by single-headed KIF1A motors

- Team work of single-headed KIF1A motors to extract membrane tubes from giant unilamellar vesicles.
- ~15 KIF1A motors can extract tubes in similar conditions to conventional kinesin, despite having a stall force 60 time smaller.

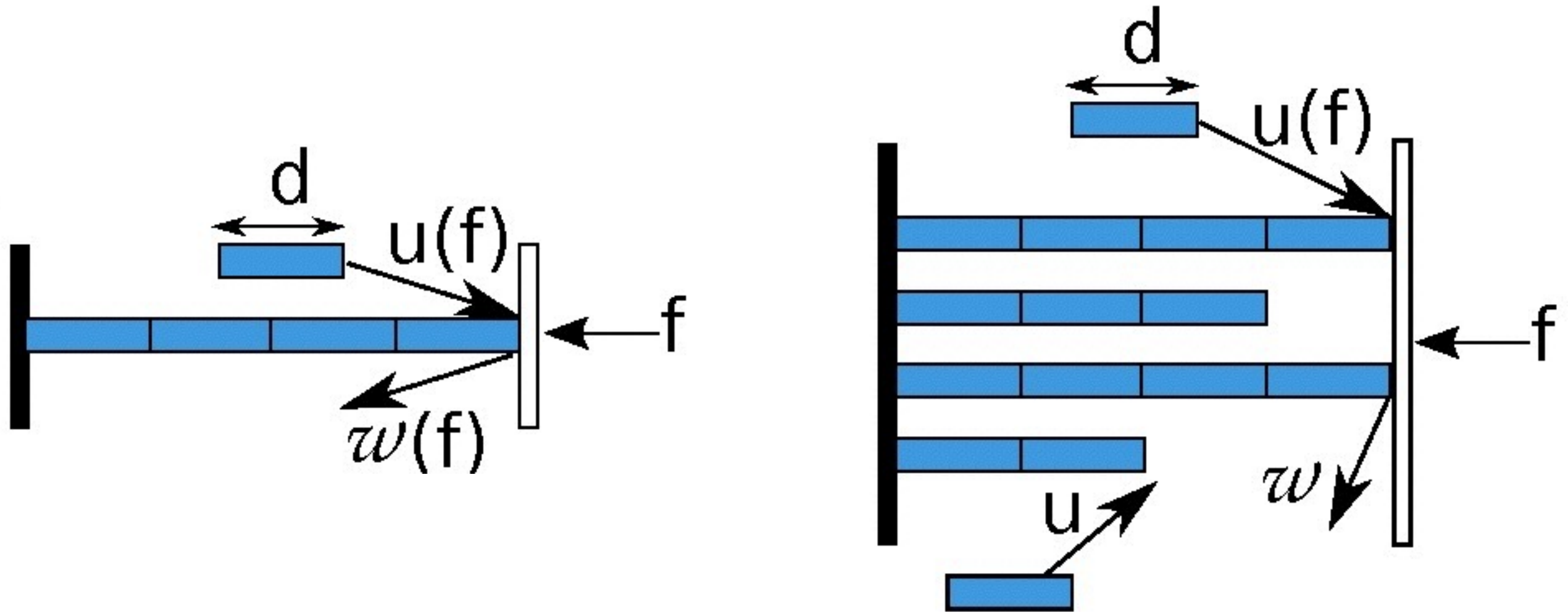




In vivo dynein attaches to Microtubule in pair.

Is it possible that dynein are not attaching to the MT in pair but cooperating in such a way that generates twice the force?

Simple kinetic model for bio-filaments



Editors' Suggestion

Sufficient conditions for the additivity of stall forces generated by multiple filaments or motors

Tripti Bameta, Dipjyoti Das, Dibyendu Das, Ranjith Padinhateeri, and Mandar M. Inamdar
Phys. Rev. E **95**, 022406 – Published 13 February 2017

Derivation for stall formula using textbook stat mech.

- System is at equilibrium at stall
- Probability distribution of the wall-position for single filament

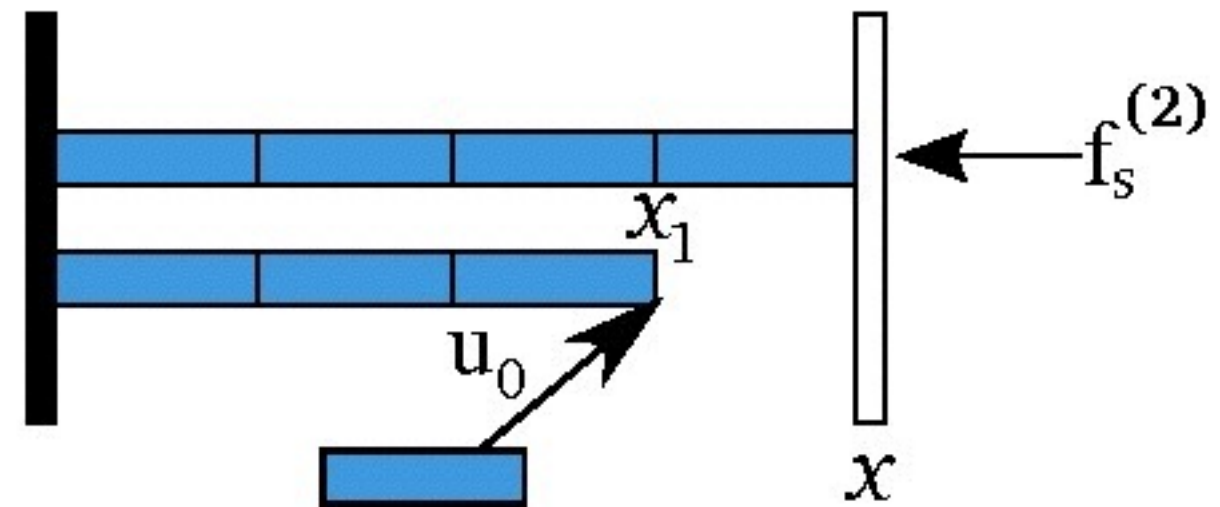
$$P(x) = \frac{1}{Z} e^{\beta f_s^{(1)} x} e^{-\beta \epsilon x}$$
$$= \frac{1}{Z} e^{\beta (f_s^{(1)} - \epsilon) x}$$

Here,

$$\epsilon = \ln \left(\frac{u}{w} \right)$$

$P(x)$ is expected not to depend on

$$f_s^{(1)} = \epsilon$$



Probability distribution of the wall-position for two filament system

$$P(x) = \frac{1}{Z} e^{\beta f_s^{(2)} x} e^{\beta \epsilon} \left(2 \sum_{x_1=0}^x e^{\beta \epsilon x_1} - e^{\beta \epsilon x} \right) \sim e^{\beta (f_s^{(2)} - 2\epsilon) x}$$

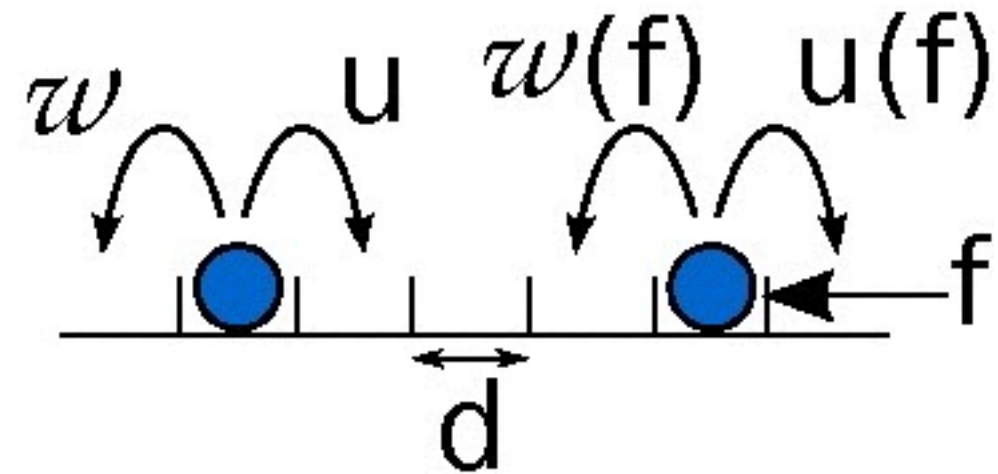
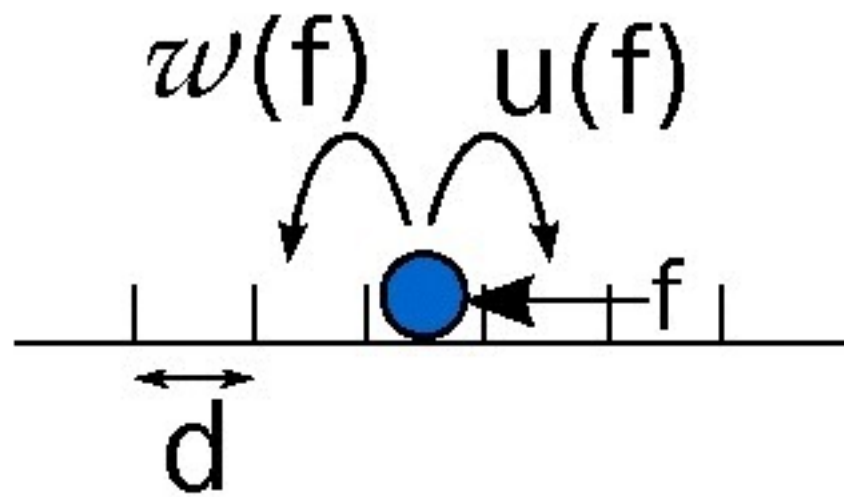
$P(x)$ is expected not to depend on x

$$f_s^{(2)} = 2\epsilon = 2f_s^1$$

This argument can be easily extended to $N > 2$

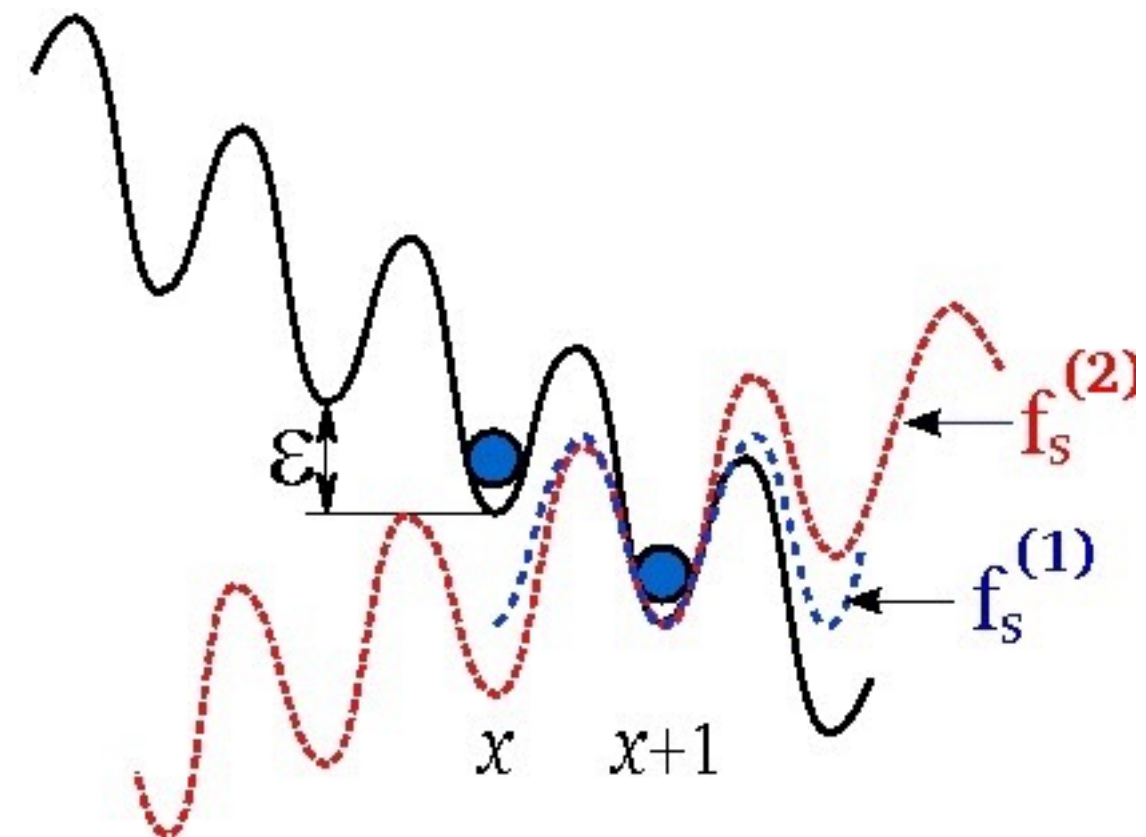
$$f_s^{(N)} = N f_s^{(1)}$$

Simple kinetic model for molecular motors



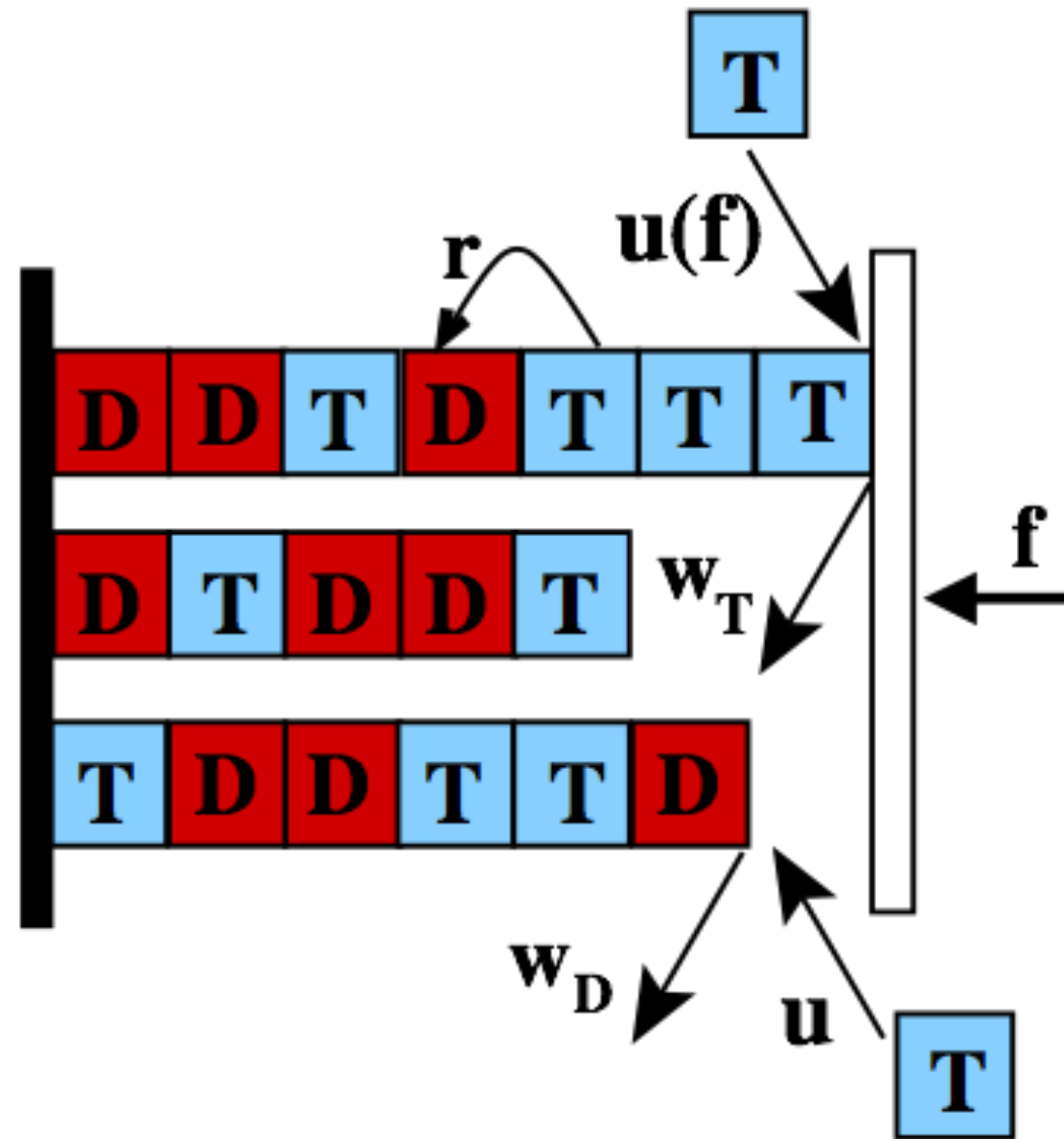
$$P(x) = \frac{1}{Z} e^{-\beta f_s^{(2)} x} e^{\beta \epsilon x} \left(\sum_{x_1=0}^{x-1} e^{\beta \epsilon x_1} \right)$$

$$\sim e^{-\beta (f_s^{(2)} - 2\epsilon) x}, \text{ for large } x.$$

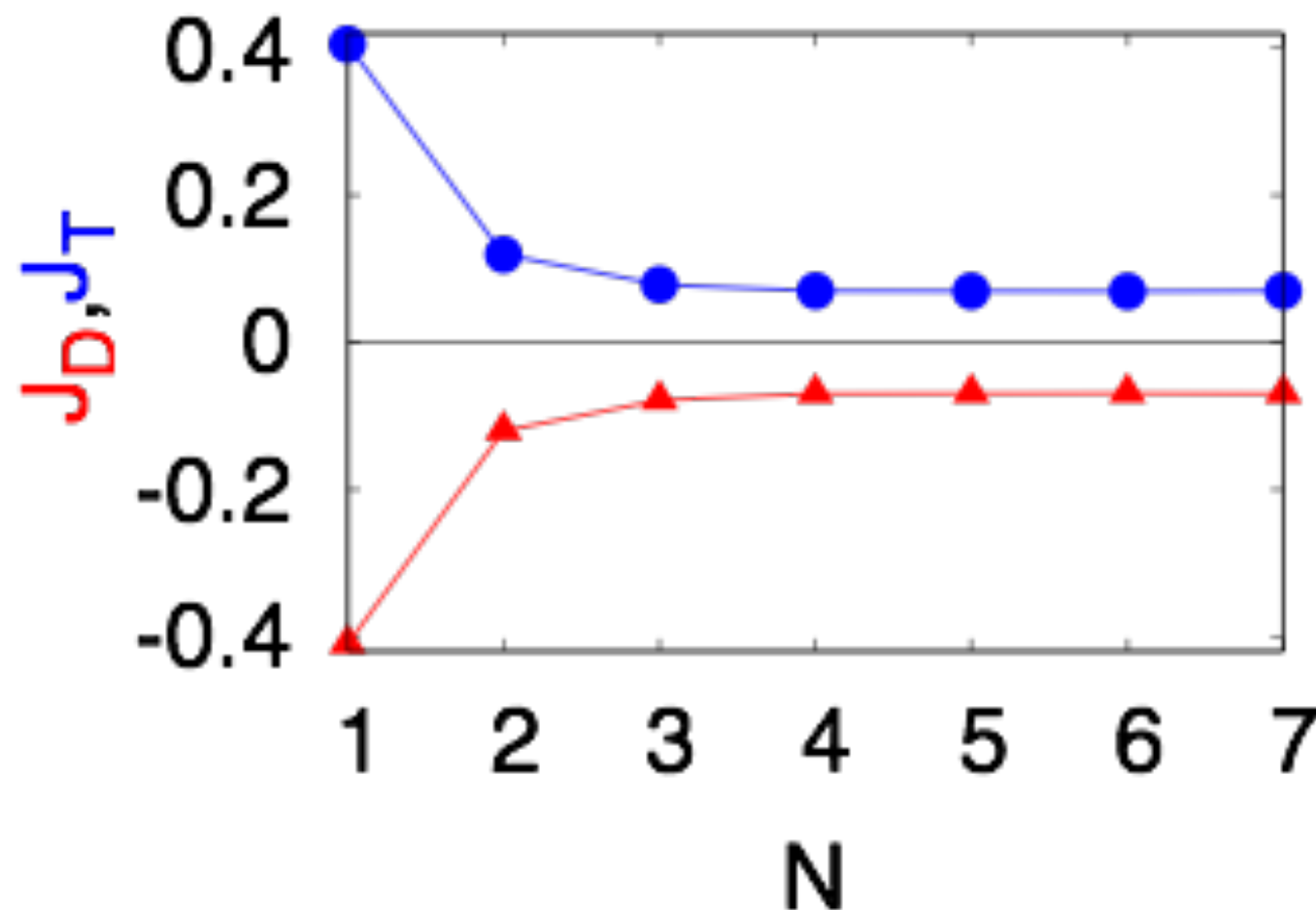


**Stall force is additive for
simple models**

Random hydrolysis model

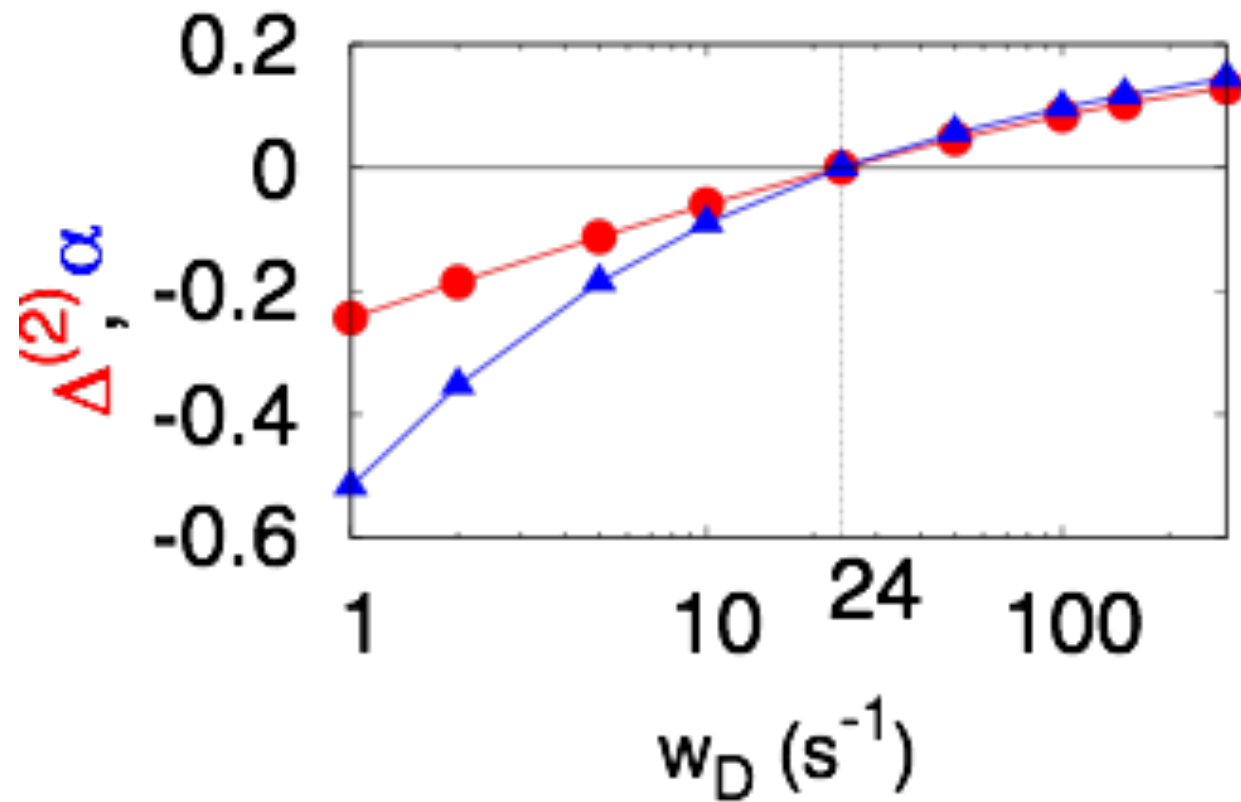


Random hydrolysis model



System with larger number of filament is closer to equilibrium

Random hydrolysis model



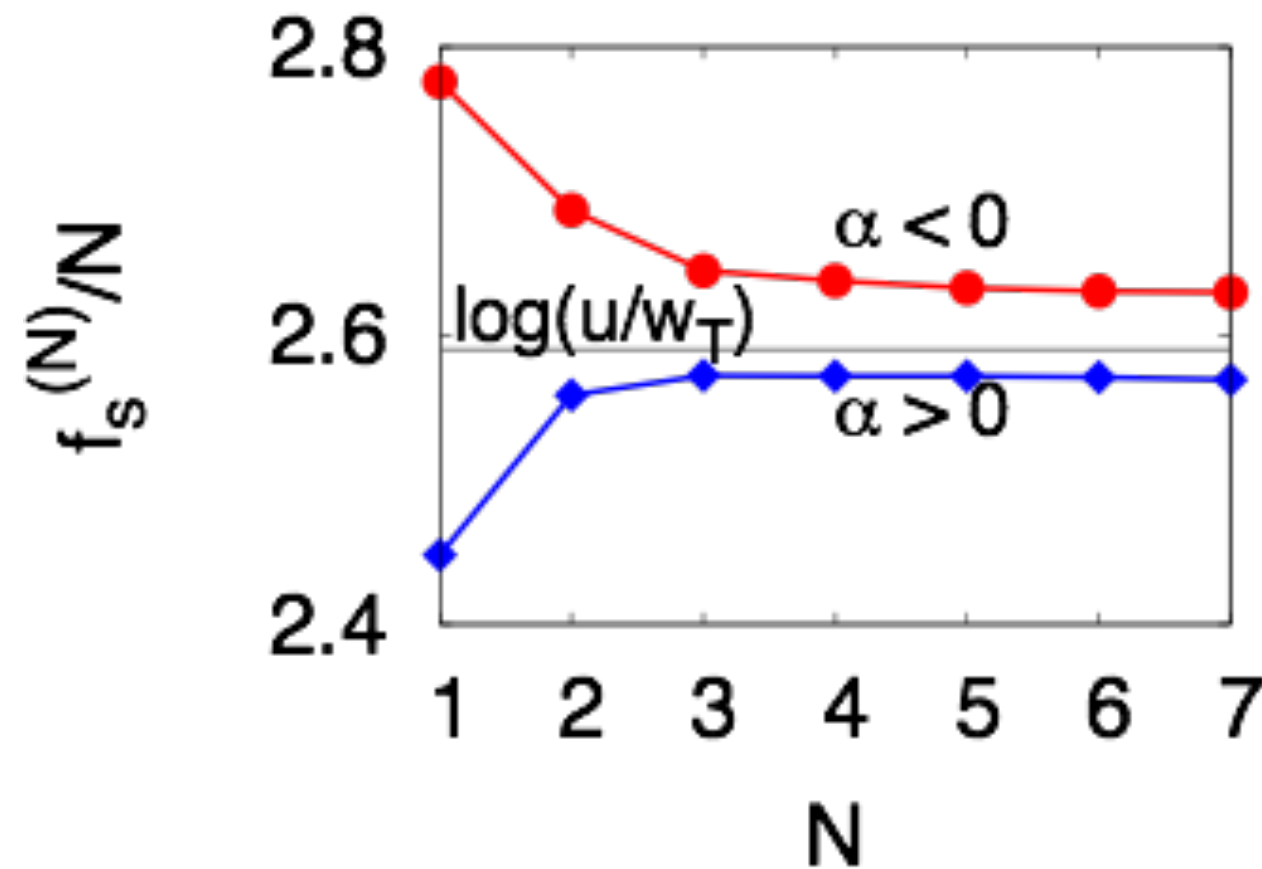
$$\Delta_2 = f_s^{(2)} - 2f_s^{(1)}$$

$$\alpha = F_{poly} - W_{poly}^{max}$$

$$= \ln \left(\frac{u}{W_T} \right) - f_s^{(1)}$$

$u = k_0 c, k_0 = 3.2 \mu M^{-1} s^{-1},$
 $c = 100 \mu M, w_T = 24 s^{-1},$
 and $r = 0.2 s^{-1}$

Random hydrolysis model



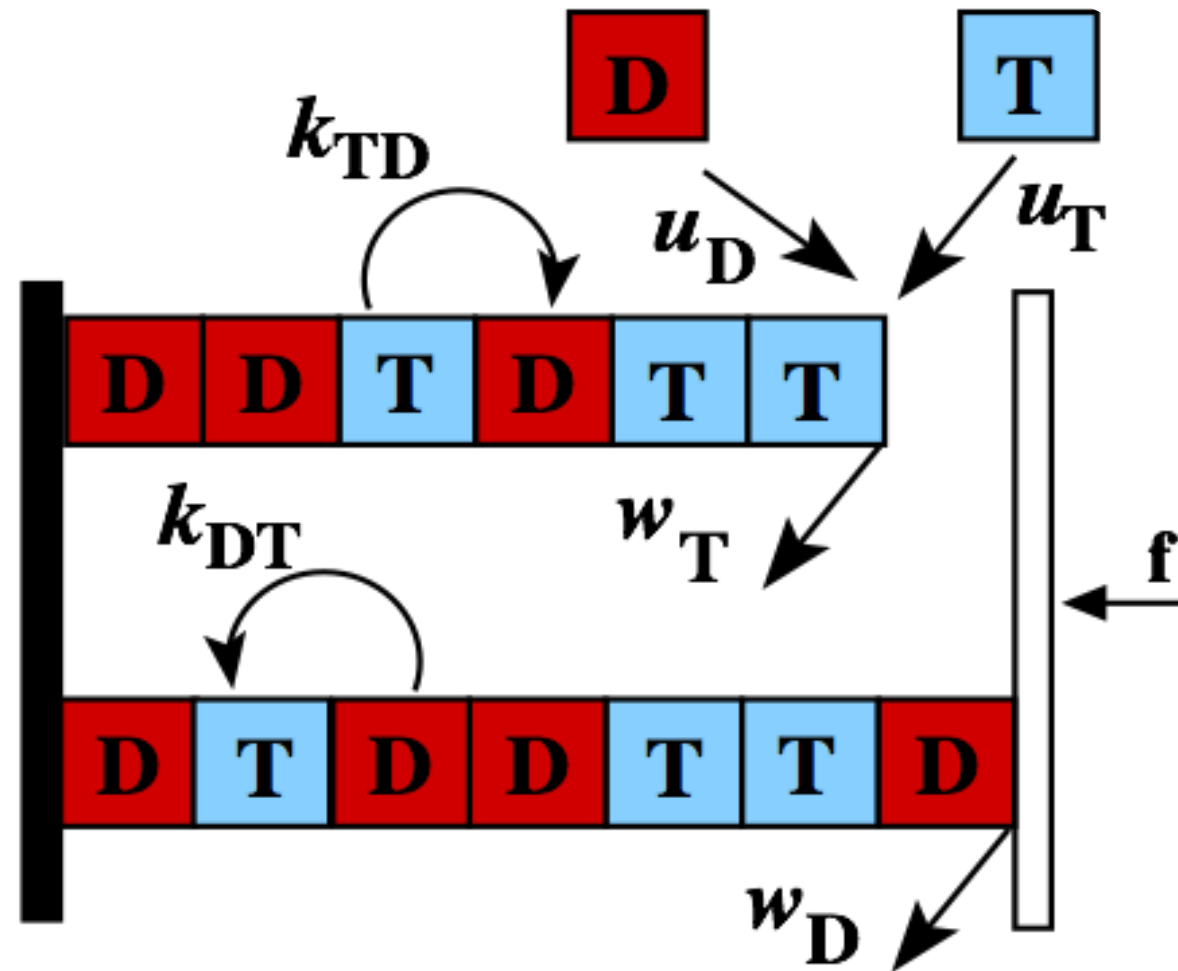
$$\alpha > 0 \quad (w_D = 290s^{-1})$$

$$\alpha < 0 \quad (w_D = 5s^{-1})$$

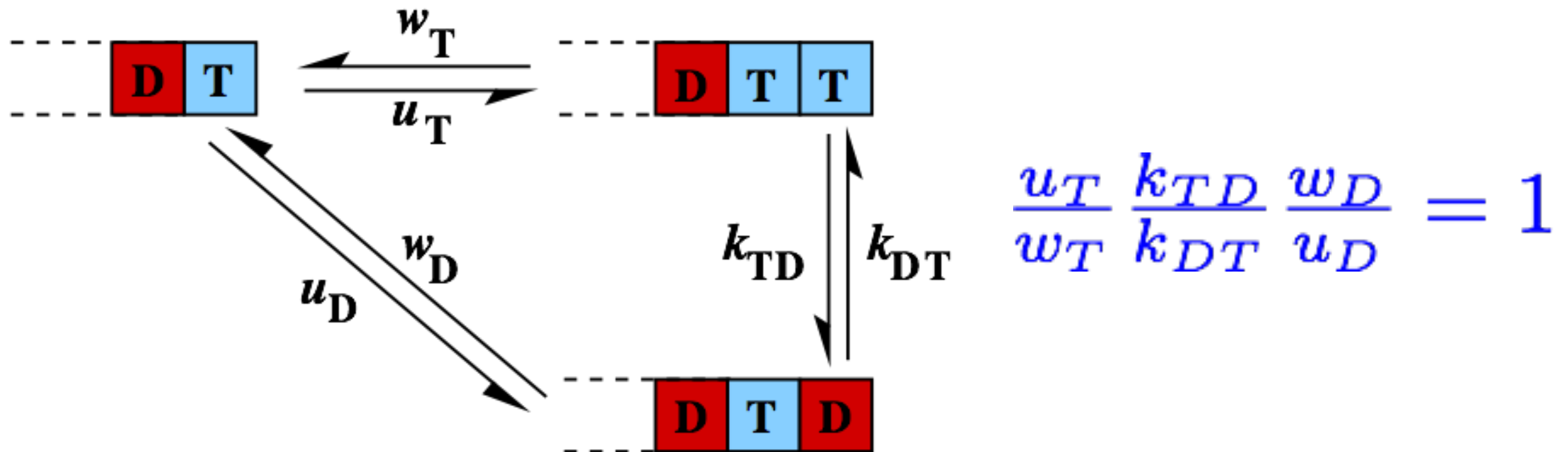
Stall forces are non-additive for biologically relevant
non-equilibrium models

detailed balance \leftrightarrow thermal
equilibrium \leftrightarrow stall force additivity

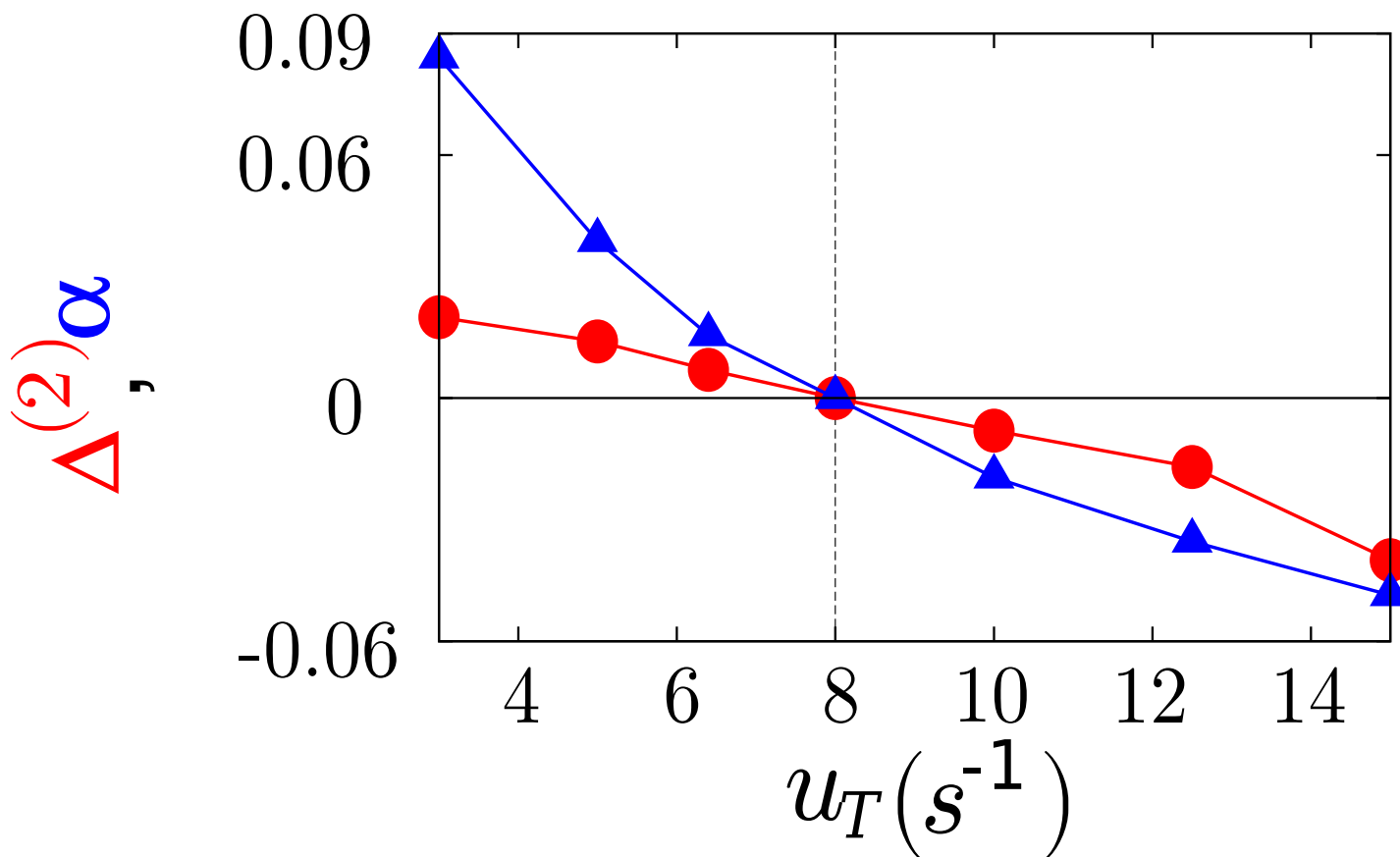
Reversible hydrolysis model



Reversible hydrolysis model



Reversible hydrolysis model

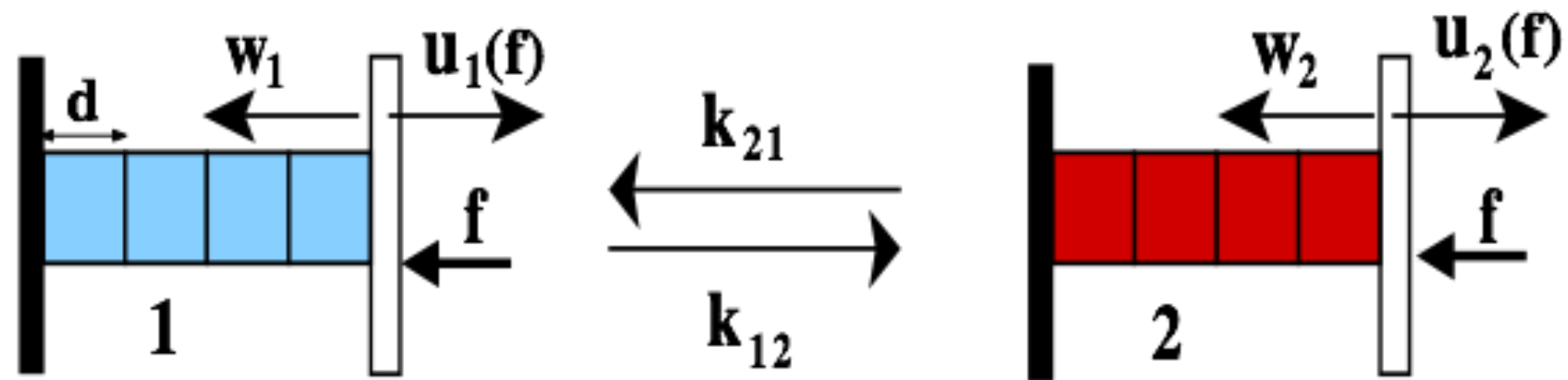


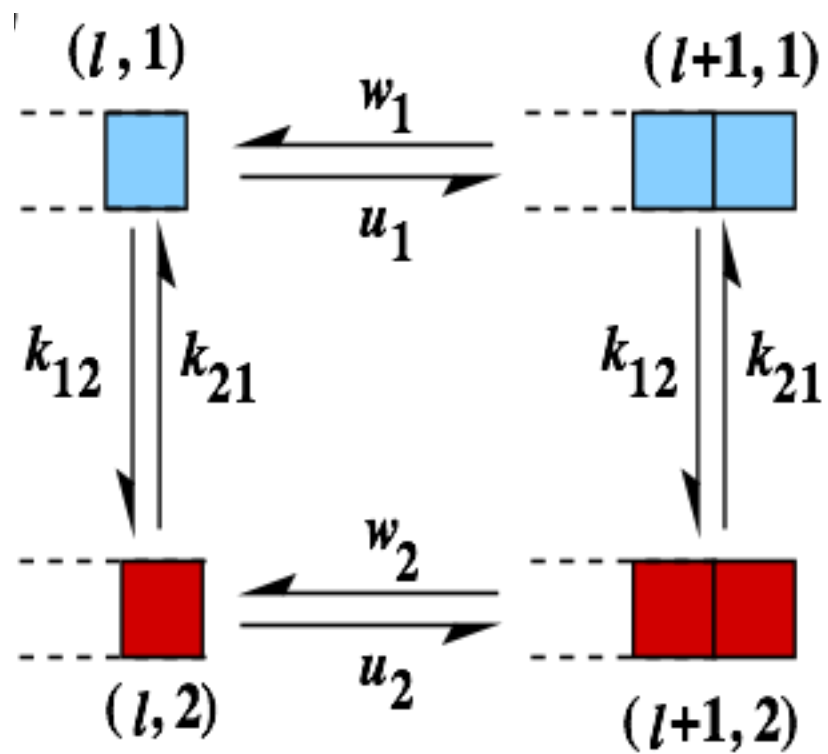
$$w_T = 2s^{-1}, k_{TD} = 0.3s^{-1}, \\ k_{DT} = 0.4s^{-1}, u_D = 3s^{-1}, \\ \text{and } w_D = 1s^{-1}$$

$$\alpha = \ln \left[\left(\frac{u_T}{w_T} \right) + \left(\frac{u_D}{w_D} \right) \right] - f_s^{(1)}$$

from the equilibrium condition at $\Delta^{(2)} = 0$ at $u_T = 8s^{-1}$

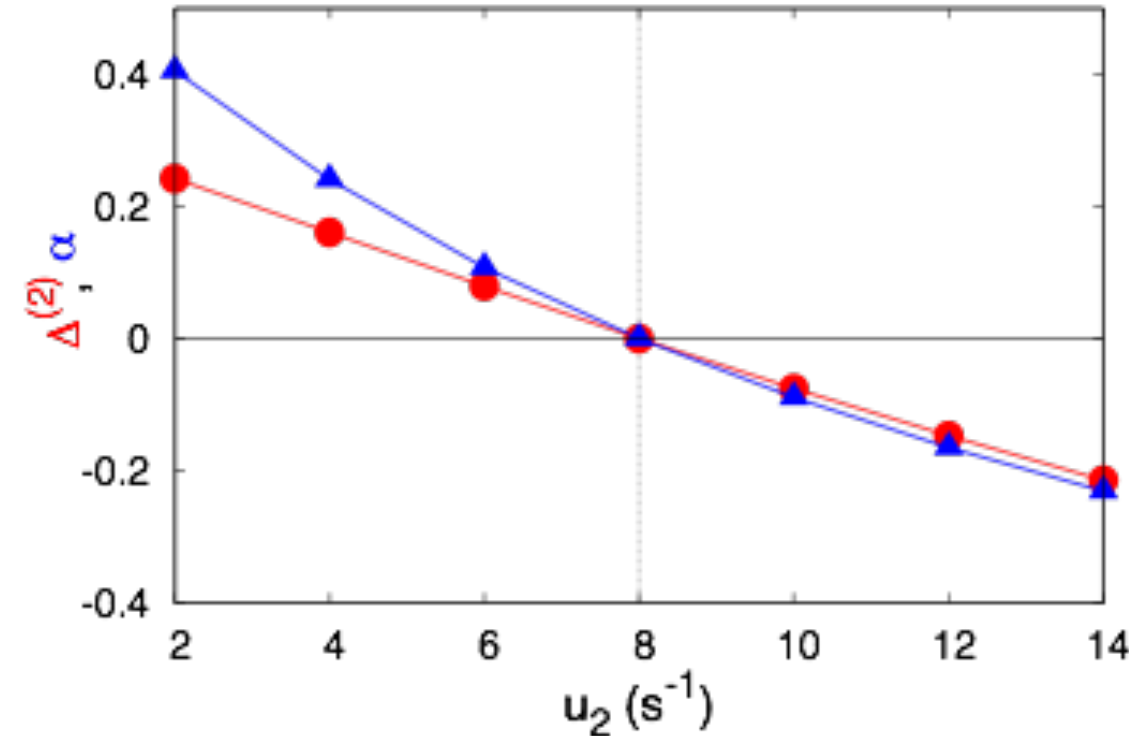
A toy model for filaments





$$u_1 k_{12} w_2 k_{21} = k_{12} u_2 k_{21} w_1$$

$$\Rightarrow \frac{u_1}{w_1} = \frac{u_2}{w_2}$$



$$\alpha = [P_1 \ln(u_1/w_1) + P_2 \ln(u_2/w_2)] - f_s^{(1)}$$

where, $P_1 = k_{21}/(k_{12} + k_{21})$ and
 $P_2 = k_{12}/(k_{12} + k_{21})$

$$k_{12} = 0.5 \text{ s}^{-1}, k_{21} = 0.5 \text{ s}^{-1},$$

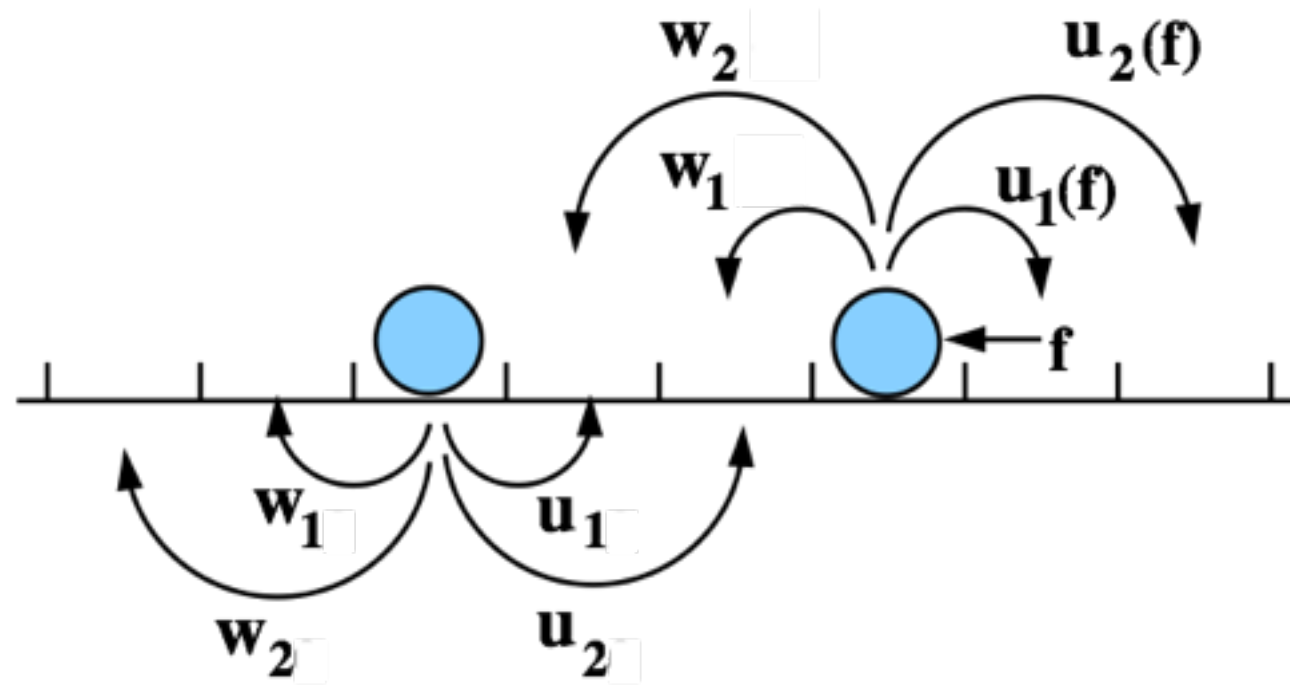
$$w_1 = 0.1 \text{ s}^{-1}, u_1 = 1 \text{ s}^{-1},$$

$$\text{and } w_2 = 0.8 \text{ s}^{-1}$$

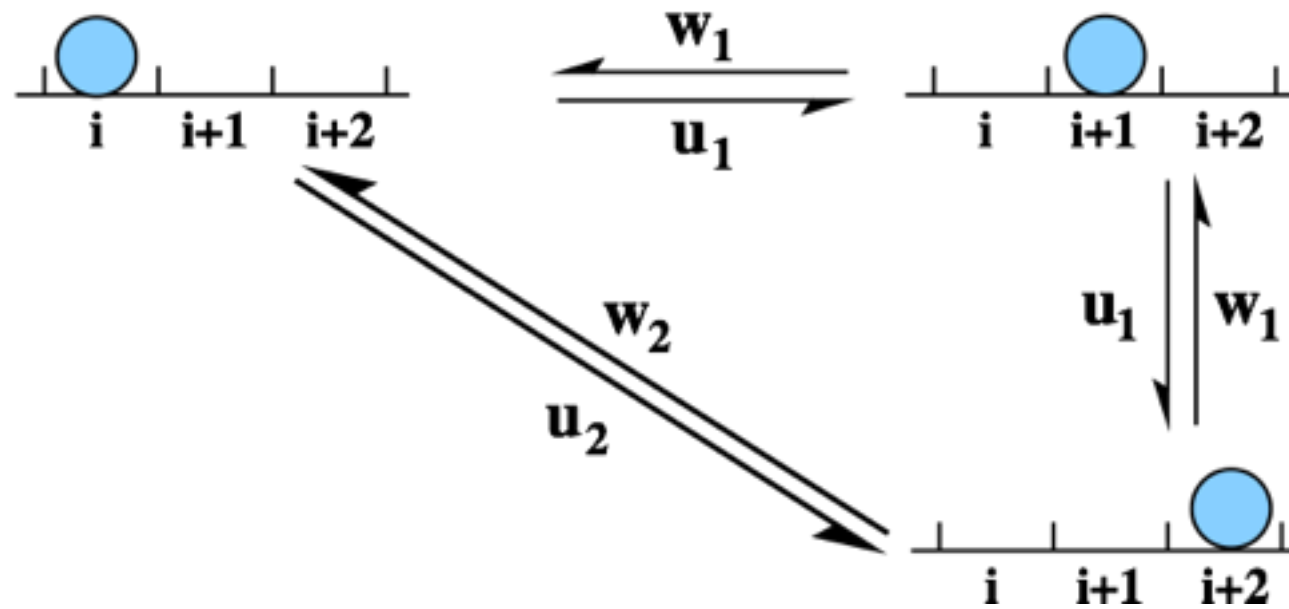
from the equilibrium condition $\Delta^{(2)} = 0$ at $u_2 = 8 \text{ s}^{-1}$

Motor Models

Multiple step-size motor

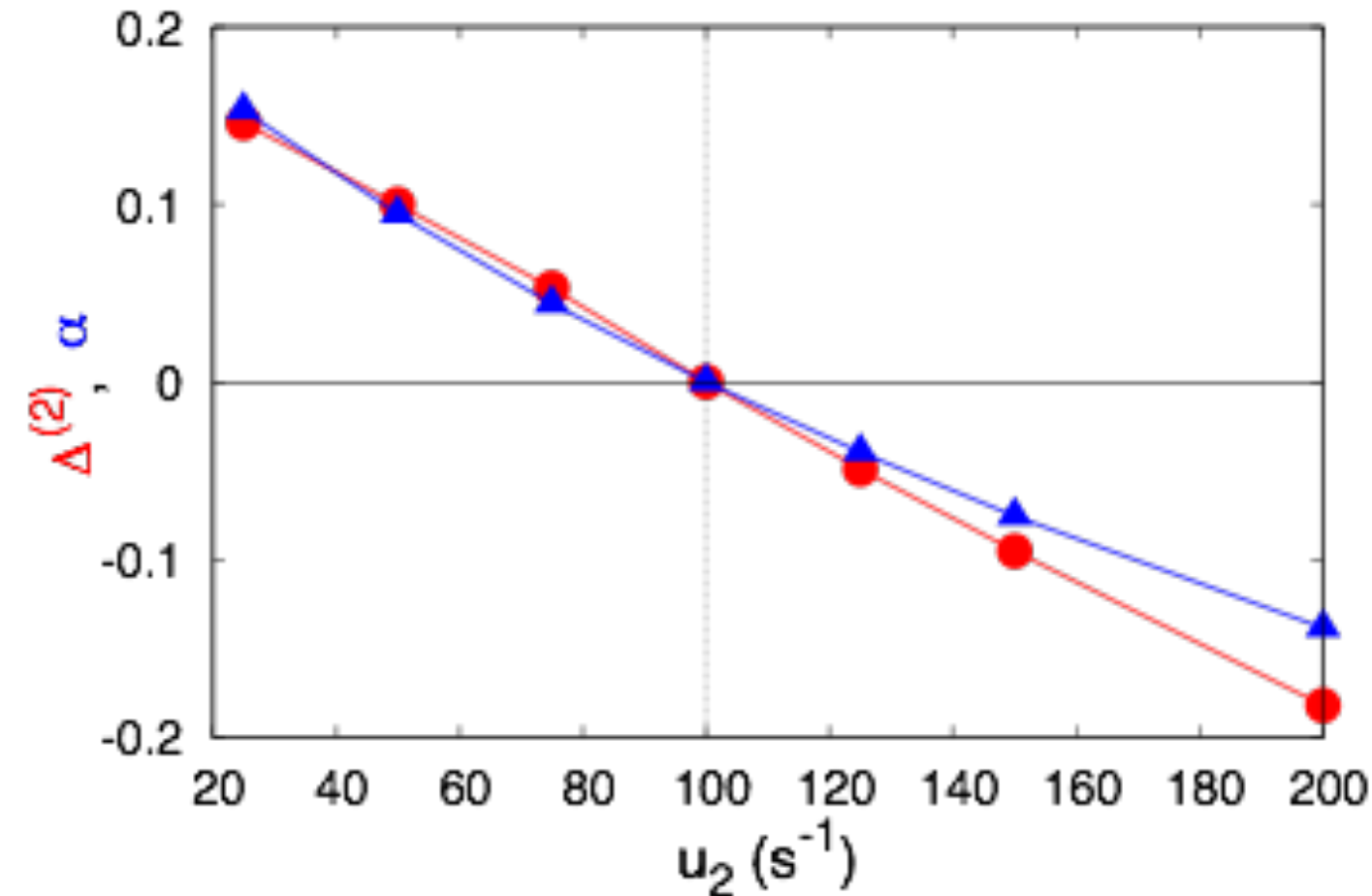


Multiple step-size motor



$$\frac{u_2}{w_2} = \left(\frac{u}{w} \right)^2$$

Multiple step-size motor

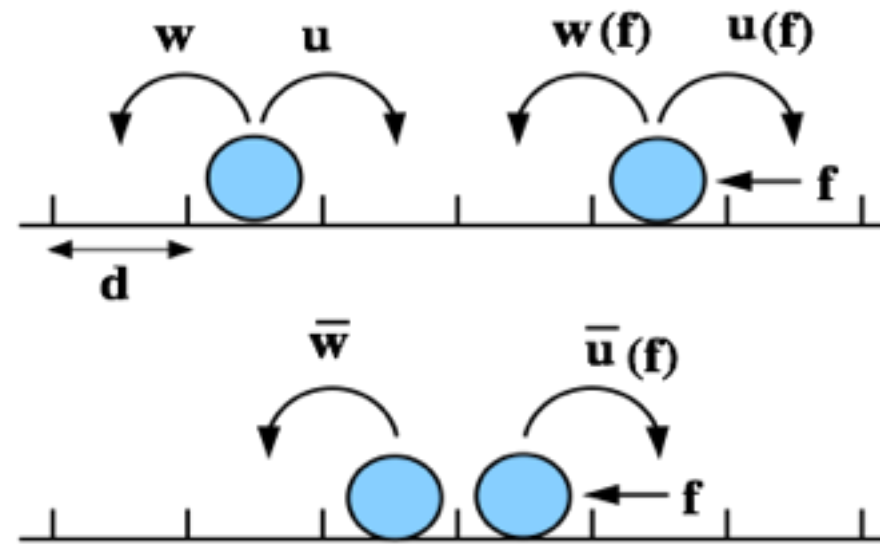


$$\alpha = \ln \left(\frac{u_1}{w_1} \right) - f_s^{(1)}$$

$$u_1 = 80s^{-1}, w_1 = 8^{-1}, \text{ and } w_2 = 1s^{-1}$$

from the equilibrium condition at $\Delta^{(2)} = 0$ at $u_2 = 100s^{-1}$

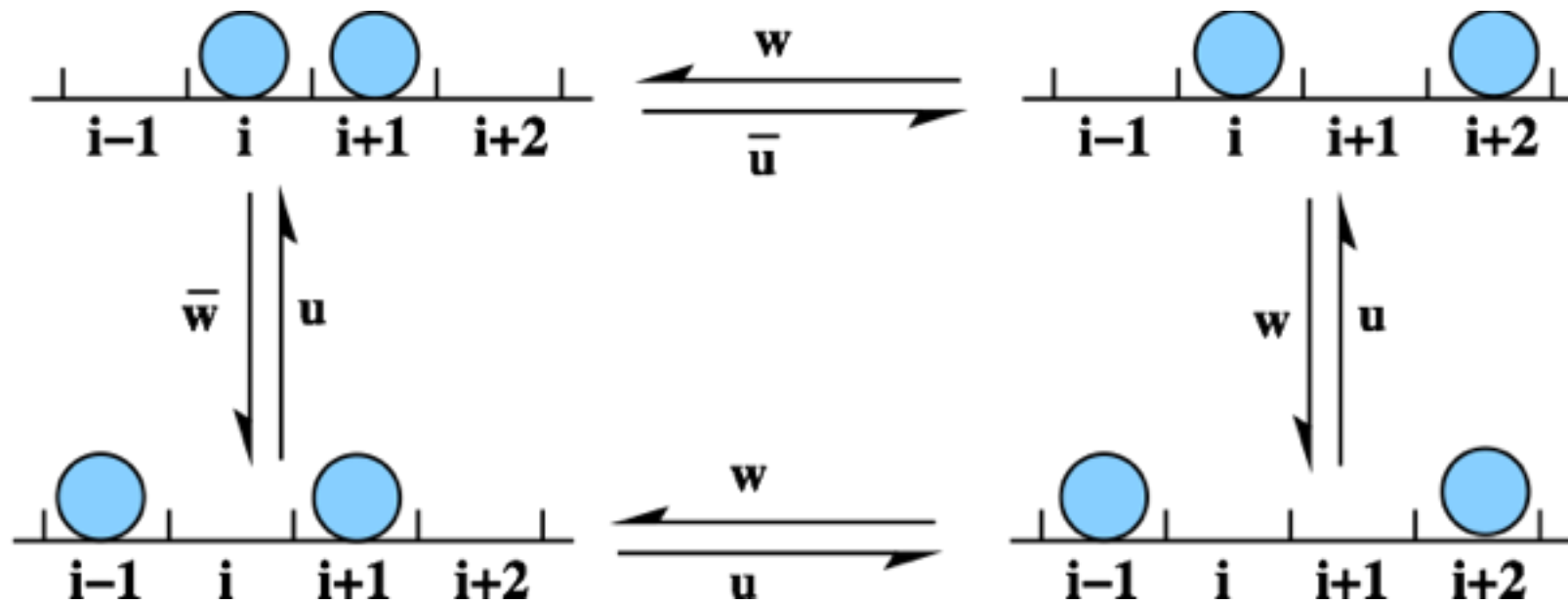
Biased random walk model for many motors



$$f_s^{(2)} = \ln \left(\frac{u\bar{u}}{w\bar{w}} + \frac{w}{u} - \frac{\bar{u}}{\bar{w}} \right)$$

$$\frac{u}{w} = \frac{\bar{u}}{\bar{w}} \implies f_s^{(2)} = 2f_s^{(1)}$$

Biased random walk model for many motors

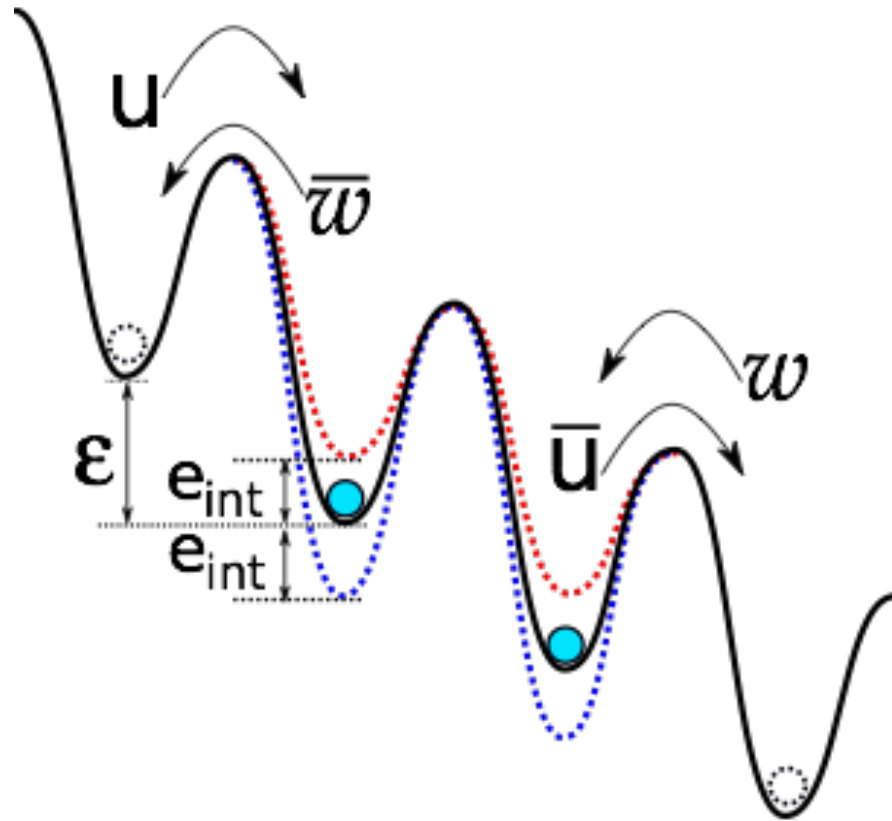


$$u.\bar{u}.w.w = \bar{w}.u.u.w$$

$$\Rightarrow \frac{u}{w} = \frac{\bar{u}}{\bar{w}}$$

Biased random walk model for many motors

Using energy landscape



$$\frac{u}{\bar{w}} = e^{\epsilon - e_{int}}$$
$$\frac{\bar{u}}{w} = e^{\epsilon + e_{int}}$$

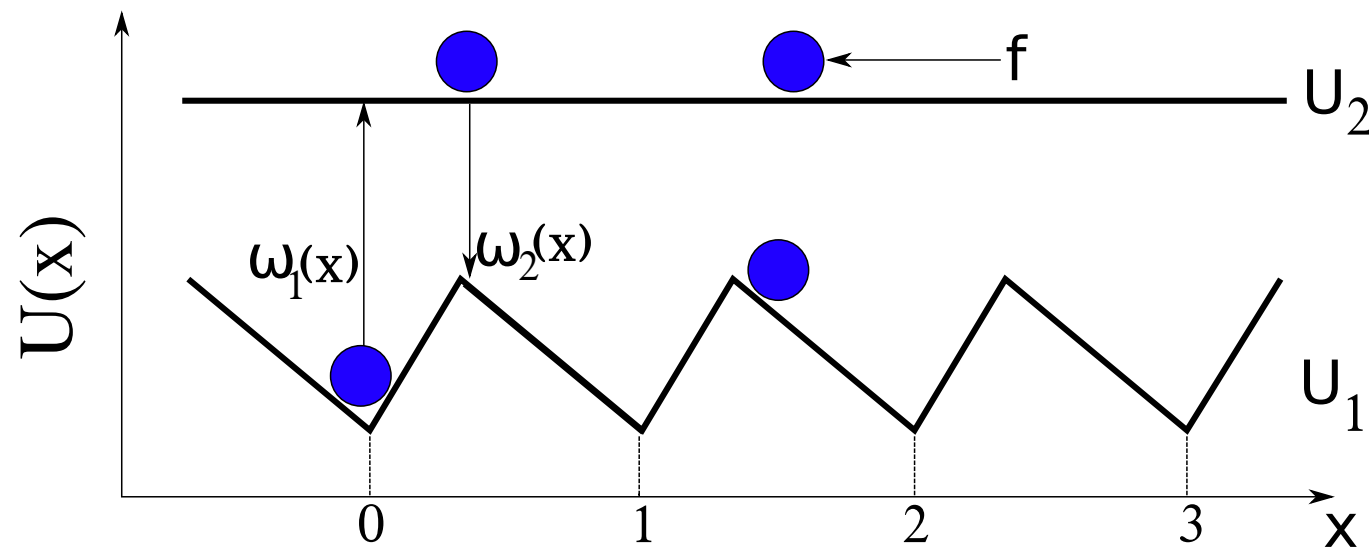
Without any interaction

$$\frac{u}{w} = e^{\epsilon}$$

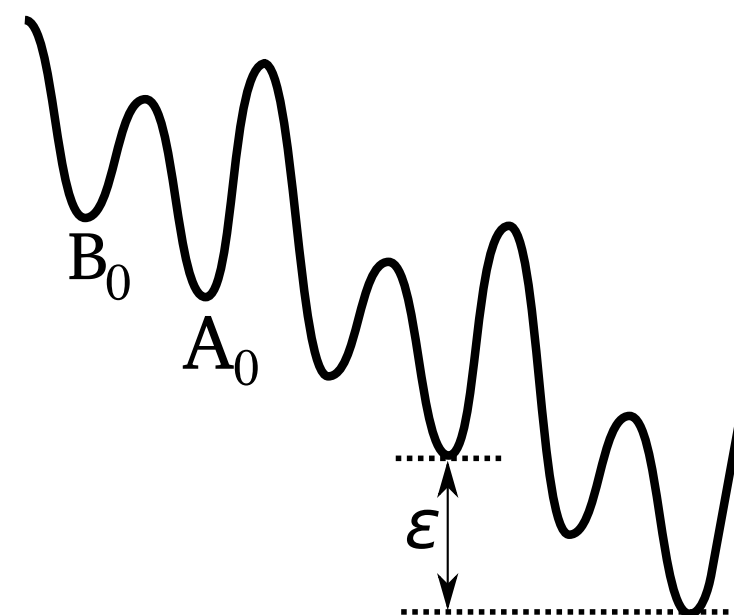
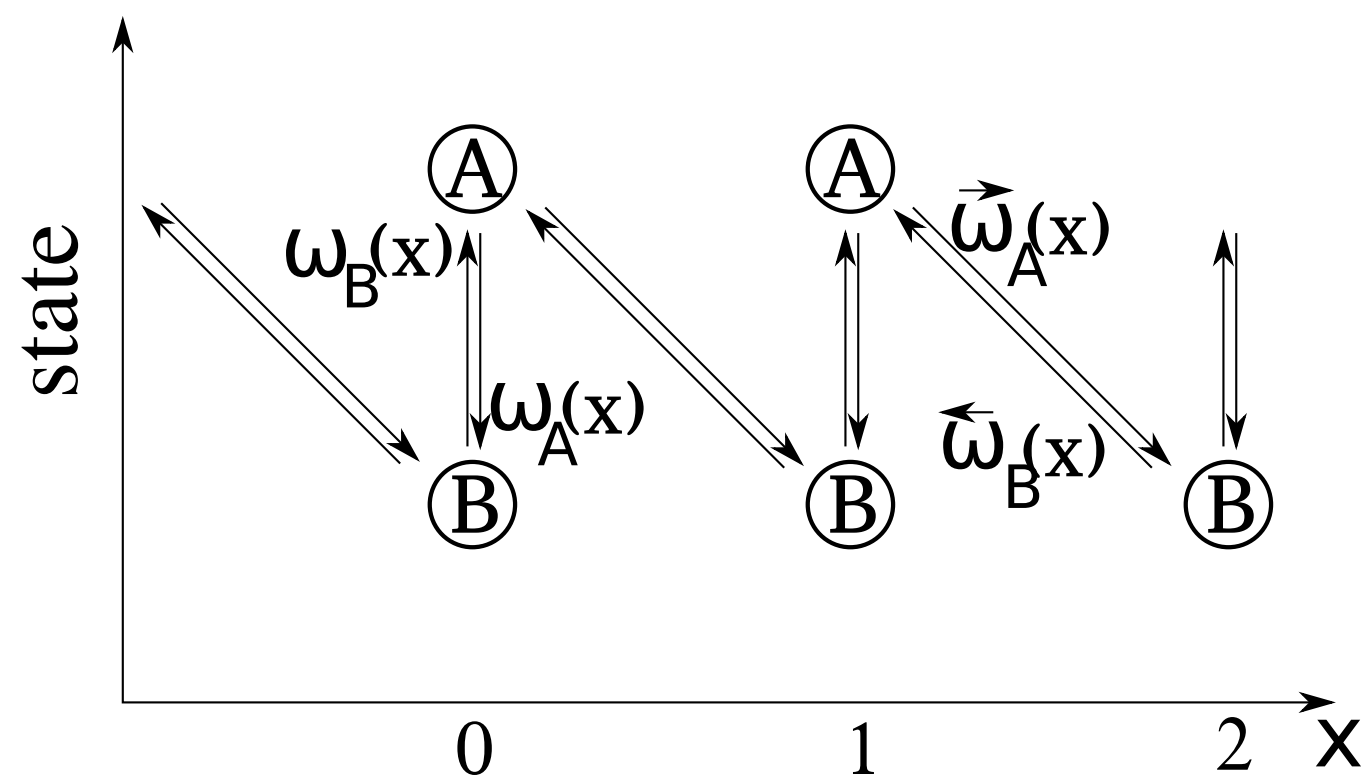
rearranging equations

$$\frac{u}{w} = \frac{\bar{u}}{\bar{w}}$$

Two-state Brownian ratchet (BR) model



Always gives enhanced cooperativity for steric interaction

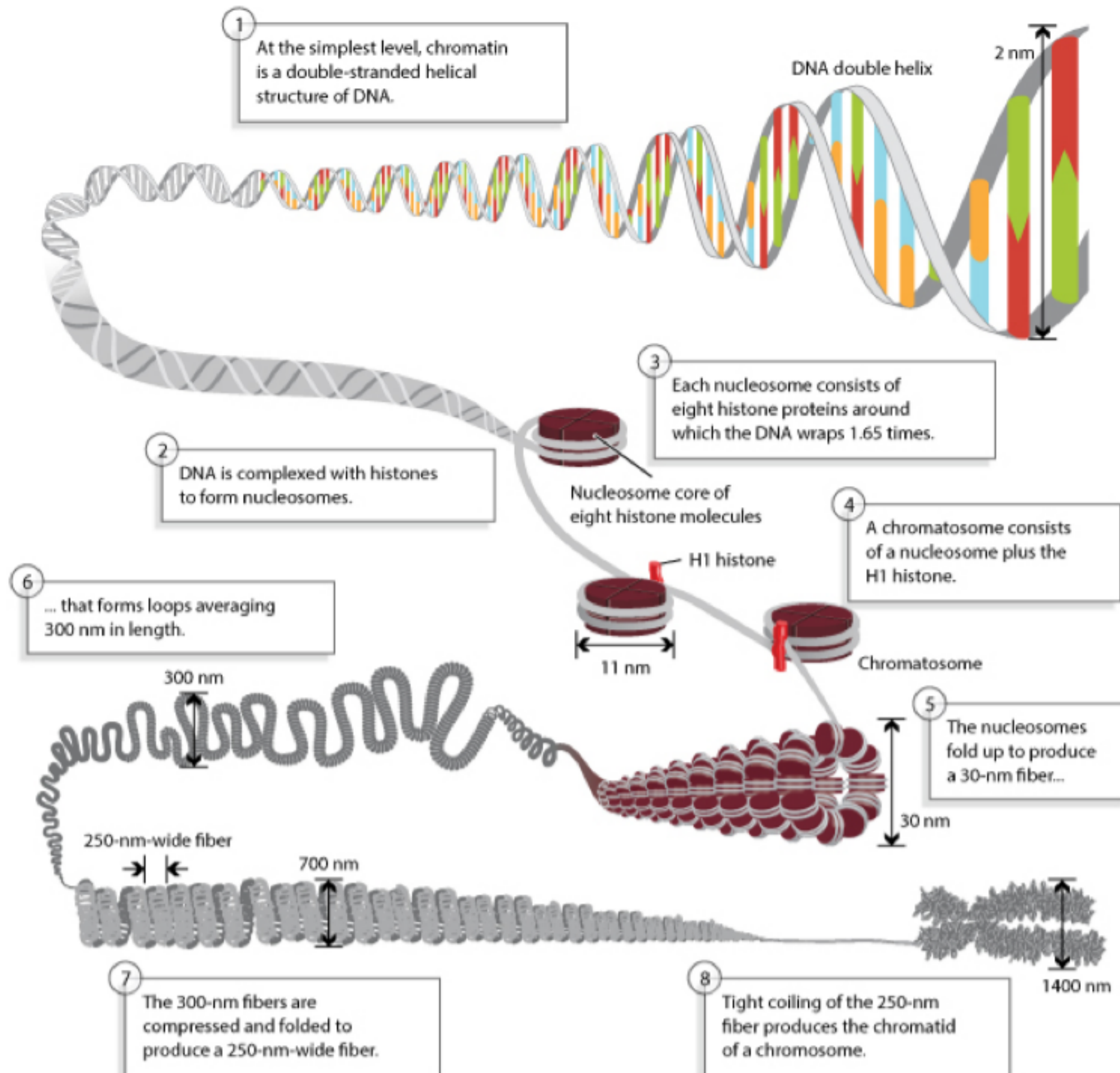


Always show force additivity, no matter how many intermediate steps are present

Conclusion

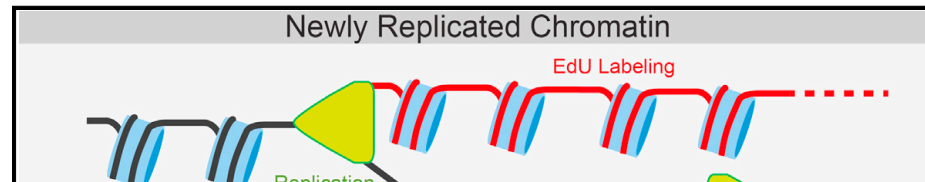
- Provides a simple description for stall force for “biased random walk” type collective motion using equilibrium arguments.
- In the presence of detailed balance for rates, stall forces for multiple filaments/motors are always additive.
- Lack of detailed balance almost always result in non-additivity of stall forces.
- In case of only one path one potential land scape, one will always get stall force additivity no matter how much intermediate steps are introduced.
- Works reasonable well for non-processive motor, as long as as long as the number of motors clustered behind the leading motor remains large enough
- Extremely broad

Mother-daughter information transfer through the
coupling of replication fork movement and
nucleosome dynamics



Transcriptional Regulators Compete with Nucleosomes Post-replication

Graphical Abstract



Authors

Srinivas Ramachandran, Steven Henikoff

Correspondence

steveh@fhcrc.org

Nucleosome positioning inheritance after replication is absolutely necessary in certain gene



Highlights

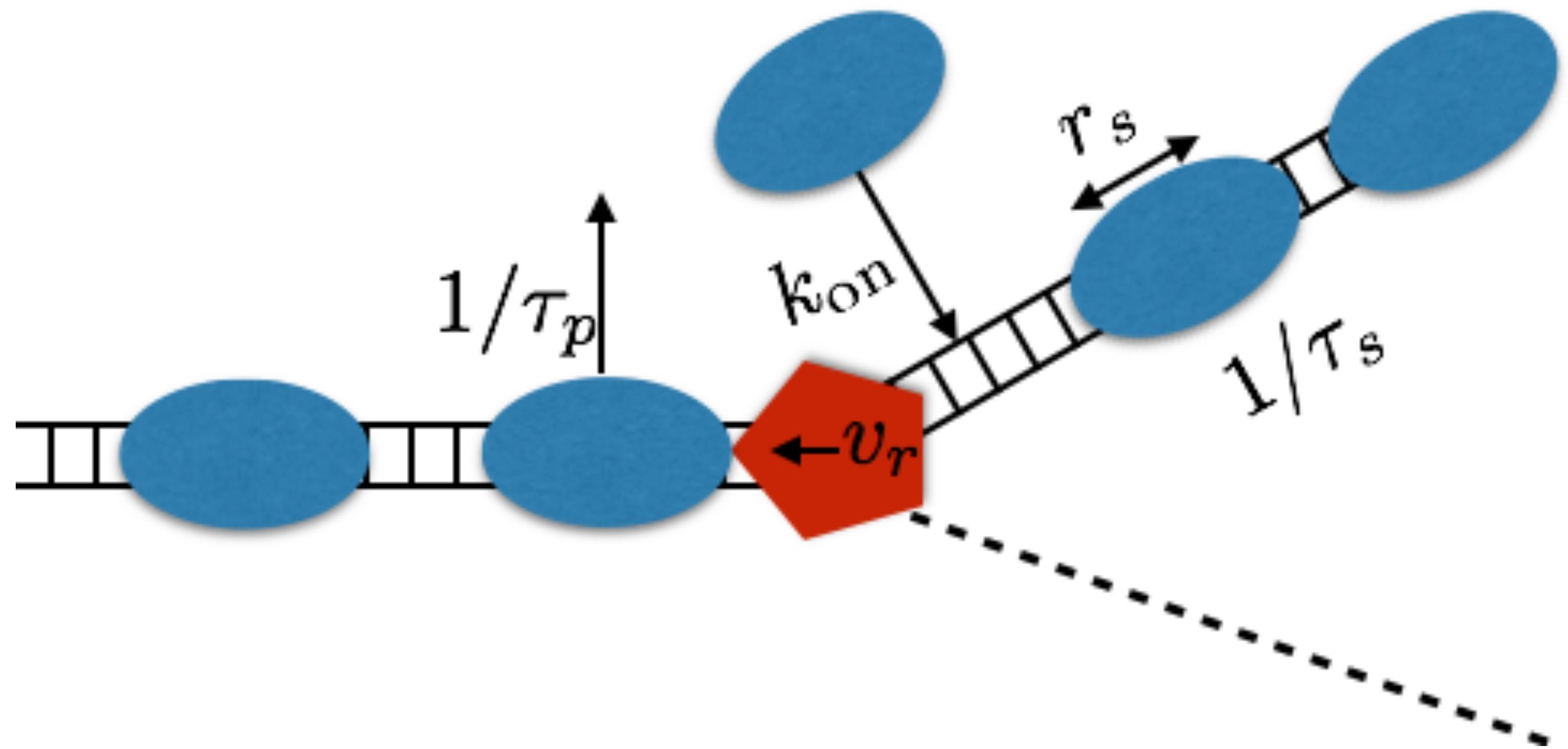
- MINCE-seq maps the nascent chromatin landscape within minutes of replication
- Nucleosomes replace transcription factors at active sites post-replication
- Nucleosome positions are conserved at inactive sites behind the replication fork
- Nucleosome gains correlate with the local abundance of transcriptional activators

Accession Numbers

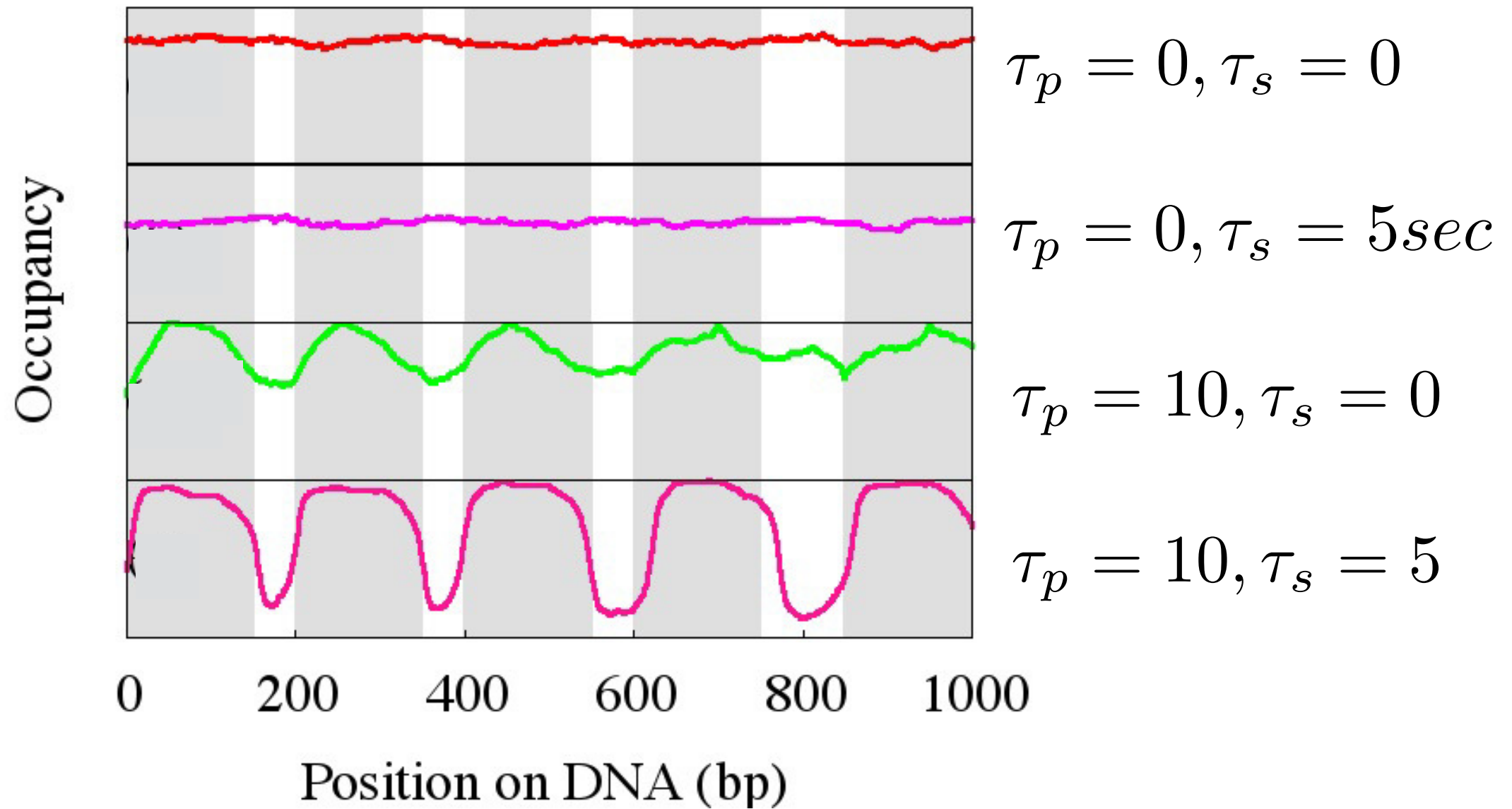
GSE76120

Is there any physical phenomenon that will help information about nucleosome positioning to be transferred from mother to daughter?

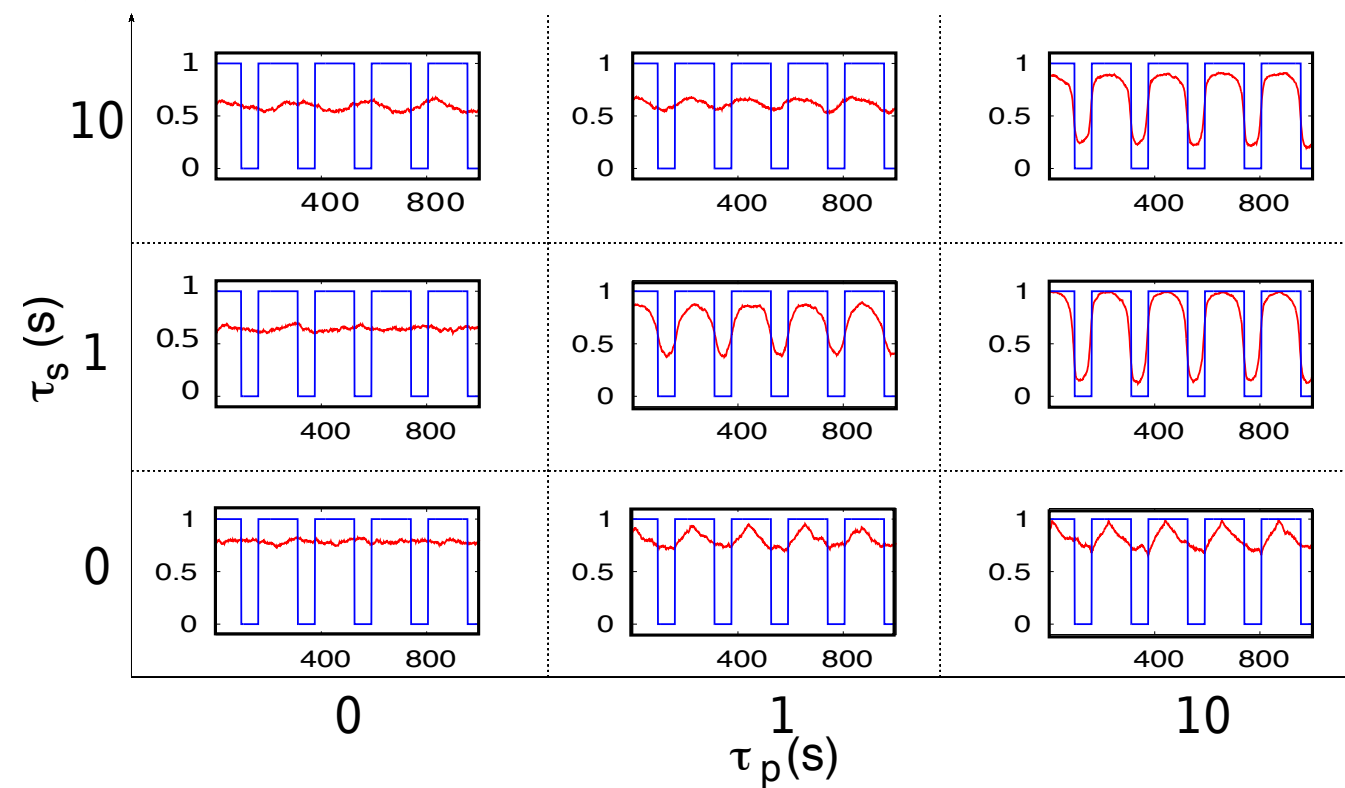
Model



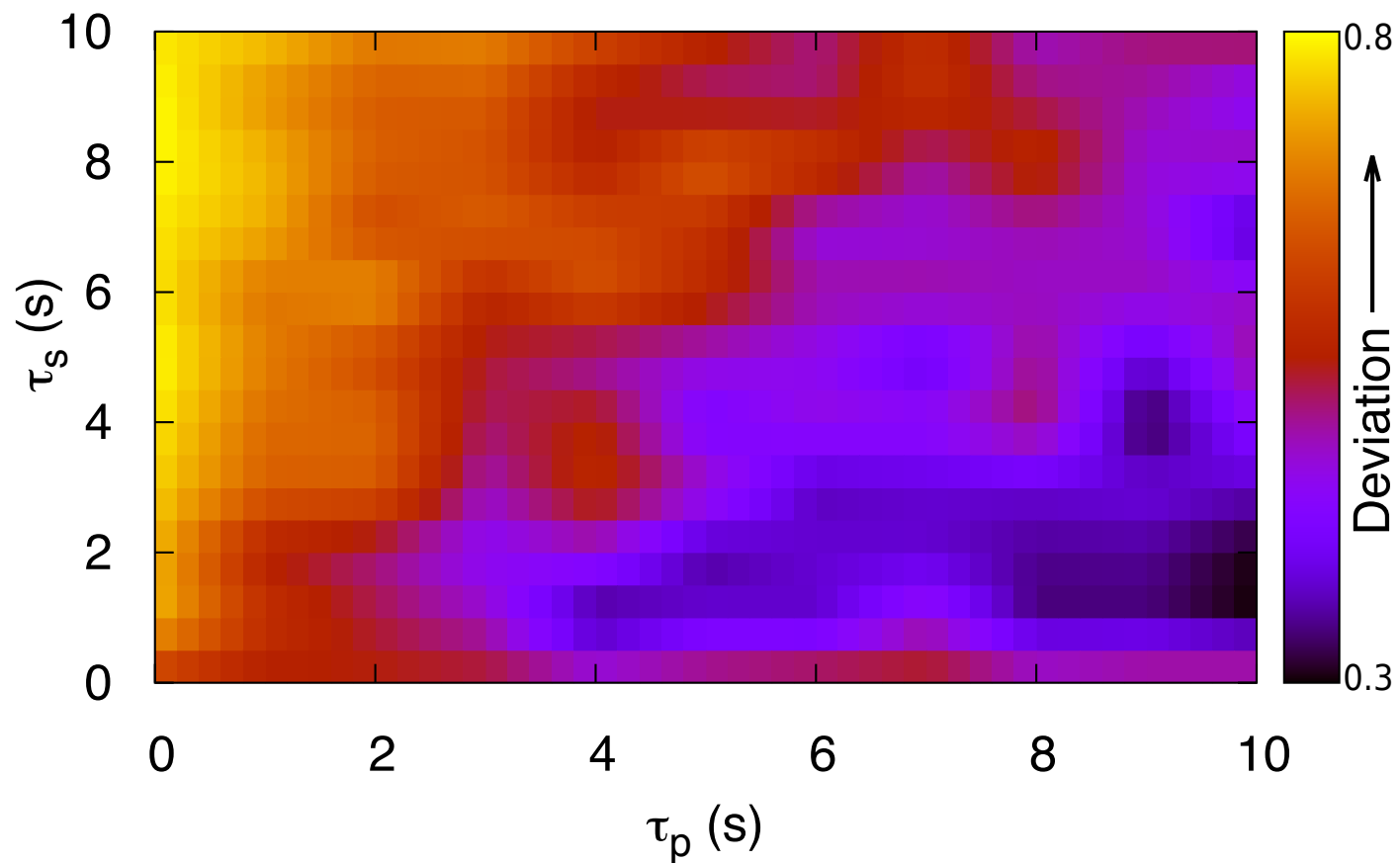
Results

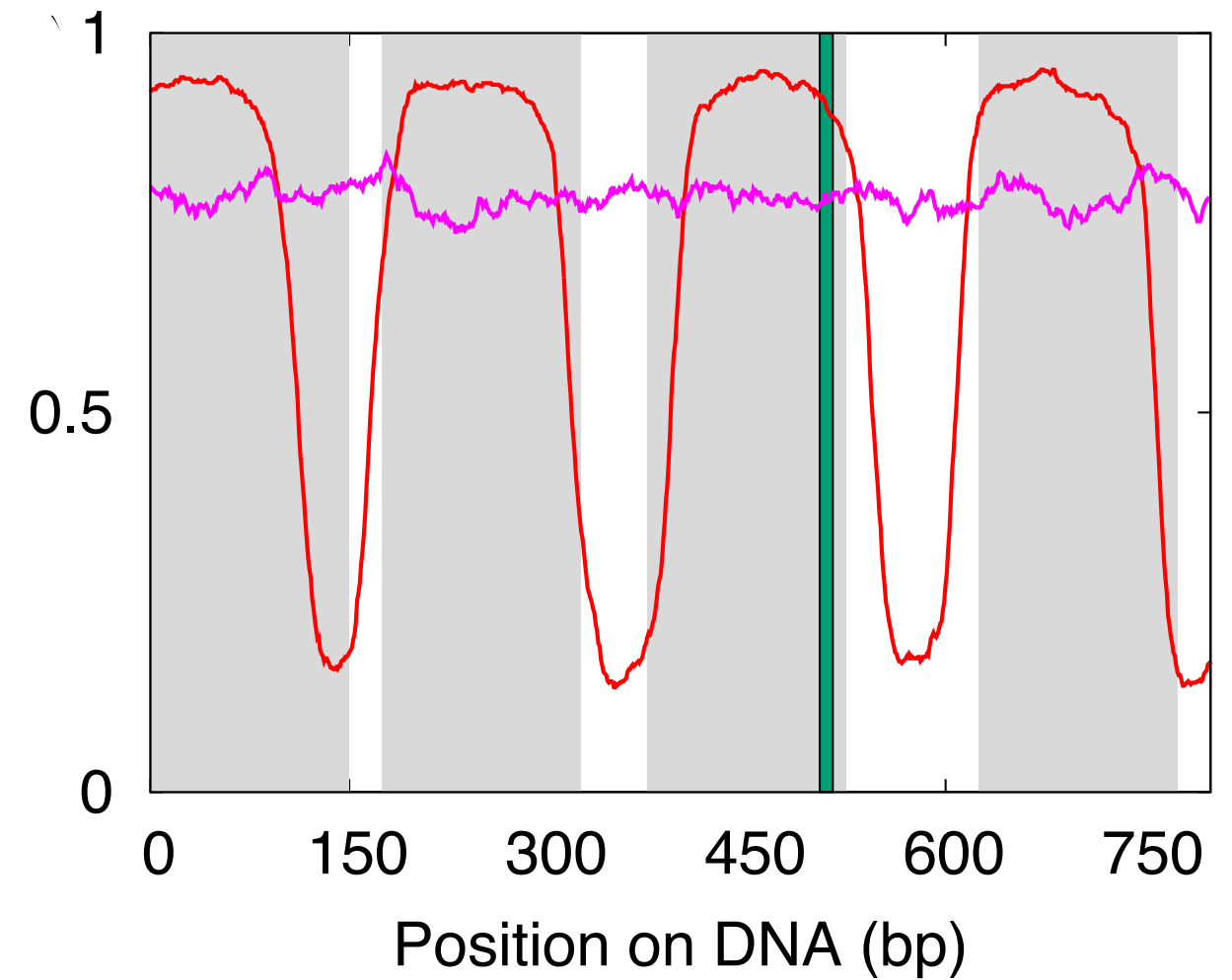
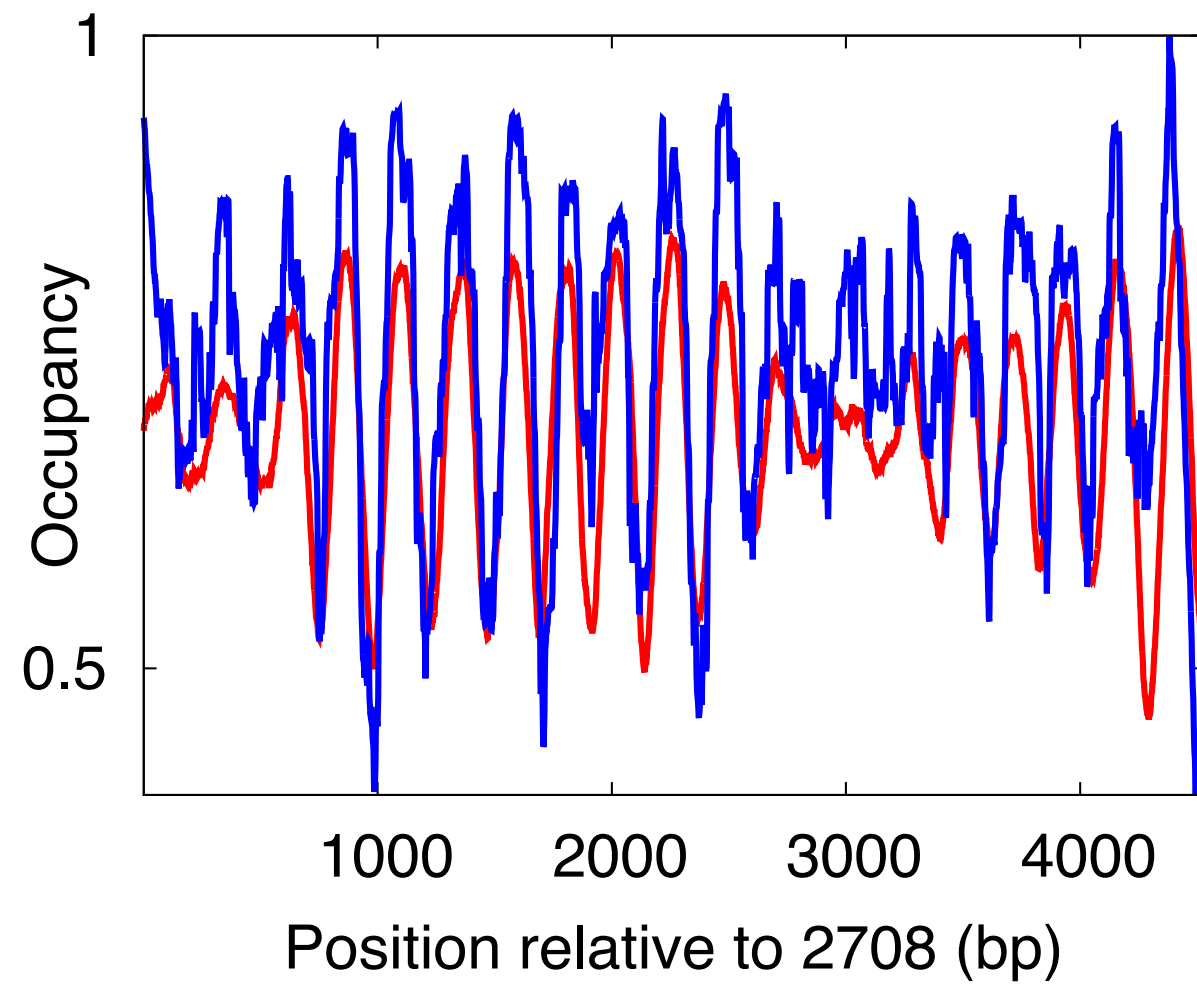


Deviation

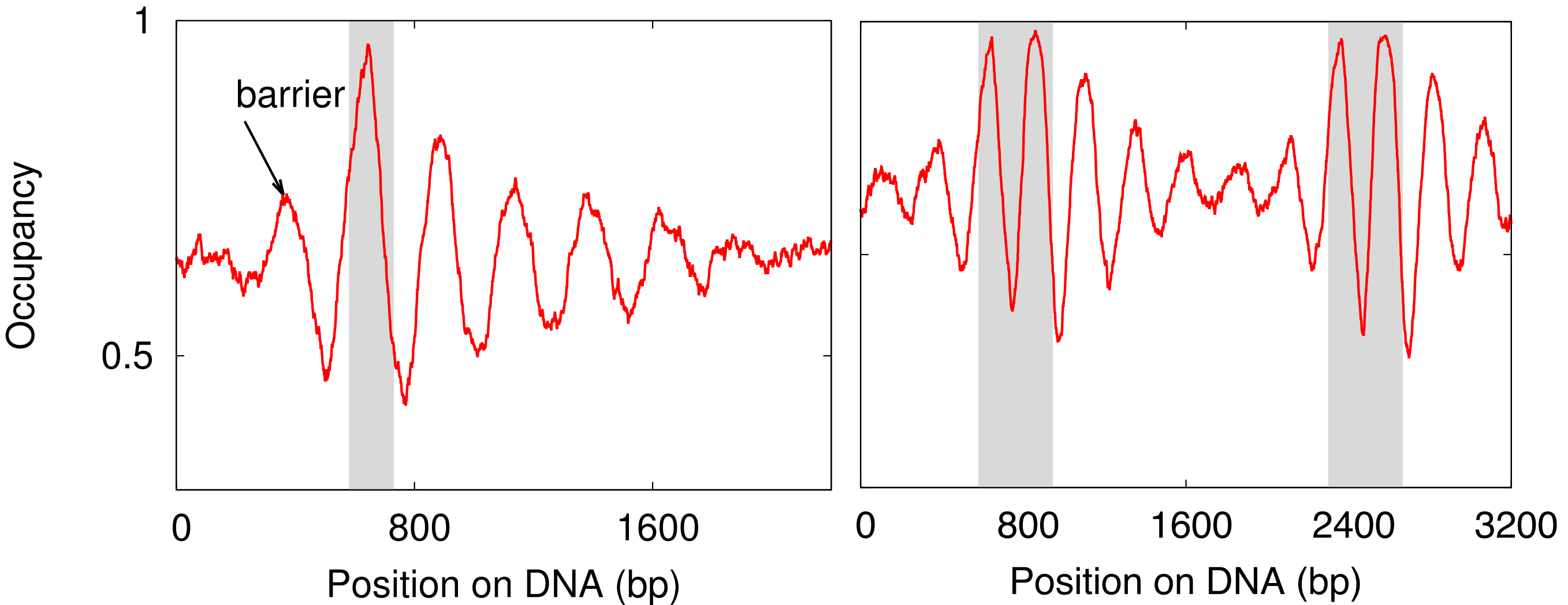


$$\chi = \sqrt{\frac{1}{L} \sum_{i=1}^L (m_i - d_i)^2}$$





Heterogeneous nucleosome organization inherited in daughter



Strongly positioned mother nucleosome gives strongly positioned daughter nucleosome

Summery

- First step towards theoretically understanding of a possible mechanism for nucleosome positioning transfer.
- Nucleosome positioning inheritance at “inactive” gene region can be produced.
- It is necessary to consider that not all the nucleosomes are well positioned and fork does not pause at all nucleosome site.
- Our results do not imply that, with pausing, the inheritance is perfect. There is some finite amount of deviation which requires further modification specially in active genes .