Pattern formation and rupture transitions in semi-flexible fiber networks with mobile cross-linkers

> P. B. Sunil Kumar Department of Physics Indian Institute of Technology Madras http://www.physics.iitm.ac.in/~sunil





Spatial and temporal organization is important for function

Nucleus is held under tension

A. Mazumder and G. V. Shivashankar Biophys. J. 93, 2209 , 2007





Mechanical cues are found to alter gene transcription, cellular differentiation in culture, and developmental programs in organisms, suggesting a strong link between cellular architecture and information control within living cells.

Formation of actin-ADF/cofilin rods transiently retards decline of mitochondrial potential and ATP in stressed neurons. Bernstein B.W. et al *Am J* Physiol Cell Physiol 291: C828–C839, 2006.

Indian Institute of Technology Kanpur



Cell stretching experiments

P. Fernadez, P. Pullarkat and A. Ott: Biophysical Journal , March 2006



3T3 Fibroblasts stuck to two micro plates coated with fiberonectin from bovine plasma



03-February-2010

Indian Institute of Technology Kanpur

Cell stretching experiments P. Fernadez, P. Pullarkat and A. Ott: Biophysical Journal , March 2006



Shearing a monolayer of Swiss 3T3 fibroblast cells



Shear rheology of a cell monolayer: P. Fernández, L. Heymann2, A. Ott, N. Aksel and P. A. Pullarkat. New Journal of Physics 9 (2007)

03-February-2010

Indian Institute of Technology Kanpur

Cytoskeleton is a dense network of polymers !

The major constituent is the Actin filaments

Actin is a polymer having a persistence length of the order of 15 μ m and thickness of about 7 nm.



Typical mesh size of the cytoskeletal network is about 100 nm Medalia et.al Science 298 1209 (2002)



03-February-2010

Indian Institute of Technology Kanpur

Building model systems : Actin networks

A state diagram for actin networks has been constructed by varying the density of cross links and the actin concentration, and showing how their changes affect the elastic modulus G_0 of the system. Gardel *et.al.* Science, **304,** 1301, (2004)



 $\rm C_s$ - concentration of cross linker

 C_{Δ} - concentration of actin

(A) R=0.0, (B) 0.07, (C) 0.5, C_A =11.9 μM





In vitro experiments have established different structural regimes in actin networks depending on α -actinin (cross linker) concentration.

The transition between these regimes are accompanied by transitions in their mechanical behavior.

O. Lieleg, M. M. A. E. Claessens and A. R. Bausch : Soft Matter - 2009



03-February-2010

Indian Institute of Technology Kanpur



03-February-2010

Indian Institute of Technology Kanpur

•Thermal undulations of a semi-flexible polymers gives rise to an "entropic elasticity" regime at small forces.



03-February-2010

Indian Institute of Technology Kanpur

•Thermal undulations of a semi-flexible polymers gives rise to an "entropic elasticity" regime at small forces.

•At large forces the response of single filaments are determined by the stretching elasticity.



03-February-2010

Indian Institute of Technology Kanpur

•Thermal undulations of a semi-flexible polymers gives rise to an "entropic elasticity" regime at small forces.

•At large forces the response of single filaments are determined by the stretching elasticity.

•This single filament response is assumed to set the network behavior



03-February-2010

Indian Institute of Technology Kanpur

•Thermal undulations of a semi-flexible polymers gives rise to an "entropic elasticity" regime at small forces.

•At large forces the response of single filaments are determined by the stretching elasticity.

•This single filament response is assumed to set the network behavior

D. A. Head, A. J. Levine, and F. C. MacKintosh, Phys. Rev. Lett. **91**, 108102 (2003) F. C. MacKintosh, J. Kas and P. Janmey PRL **75** 4425 (1995)



03-February-2010

Indian Institute of Technology Kanpur

•Thermal undulations of a semi-flexible polymers gives rise to an "entropic elasticity" regime at small forces.

•At large forces the response of single filaments are determined by the stretching elasticity.

•This single filament response is assumed to set the network behavior

D. A. Head, A. J. Levine, and F. C. MacKintosh, Phys. Rev. Lett. **91**, 108102 (2003) F. C. MacKintosh, J. Kas and P. Janmey PRL **75** 4425 (1995)

•Stiffening is caused by nonaffine network rearrangements.



03-February-2010

Indian Institute of Technology Kanpur

•Thermal undulations of a semi-flexible polymers gives rise to an "entropic elasticity" regime at small forces.

•At large forces the response of single filaments are determined by the stretching elasticity.

•This single filament response is assumed to set the network behavior

D. A. Head, A. J. Levine, and F. C. MacKintosh, Phys. Rev. Lett. **91**, 108102 (2003) F. C. MacKintosh, J. Kas and P. Janmey PRL **75** 4425 (1995)

•Stiffening is caused by nonaffine network rearrangements.

•These rearrangements govern a transition from a bending-dominated response at small strains to a stretching-dominated response at large strains.



03-February-2010

Indian Institute of Technology Kanpur

•Thermal undulations of a semi-flexible polymers gives rise to an "entropic elasticity" regime at small forces.

•At large forces the response of single filaments are determined by the stretching elasticity.

•This single filament response is assumed to set the network behavior

D. A. Head, A. J. Levine, and F. C. MacKintosh, Phys. Rev. Lett. **91**, 108102 (2003) F. C. MacKintosh, J. Kas and P. Janmey PRL **75** 4425 (1995)

•Stiffening is caused by nonaffine network rearrangements.

•These rearrangements govern a transition from a bending-dominated response at small strains to a stretching-dominated response at large strains.

•Filament undulations, which are key in the existing explanation of stiffening, merely postpone the transition.



03-February-2010

Indian Institute of Technology Kanpur

•Thermal undulations of a semi-flexible polymers gives rise to an "entropic elasticity" regime at small forces.

•At large forces the response of single filaments are determined by the stretching elasticity.

•This single filament response is assumed to set the network behavior

D. A. Head, A. J. Levine, and F. C. MacKintosh, Phys. Rev. Lett. **91**, 108102 (2003) F. C. MacKintosh, J. Kas and P. Janmey PRL **75** 4425 (1995)

•Stiffening is caused by nonaffine network rearrangements.

•These rearrangements govern a transition from a bending-dominated response at small strains to a stretching-dominated response at large strains.

•Filament undulations, which are key in the existing explanation of stiffening, merely postpone the transition.

P. R. Onck, T. Koeman, T. van Dillen, and E. van der Giessen, Phys. Rev. Lett. 95, 178192 (2005)

03-February-2010

Indian Institute of Technology Kanpur





03-February-2010

Indian Institute of Technology Kanpur

J. Astrom, P.B. S. K., M. Karttunen and I. Vattulainen Phys. Rev. E 77, 051913 (2008)



03-February-2010

Indian Institute of Technology Kanpur

J. Astrom, P.B. S. K., M. Karttunen and I. Vattulainen Phys. Rev. E 77, 051913 (2008)

•A 3D computational model that allow for changes in network geometry and account for their dynamic nature

•The model allow for the intersection points of polymers to move smoothly in three dimensions.



03-February-2010

Indian Institute of Technology Kanpur

J. Astrom, P.B. S. K., M. Karttunen and I. Vattulainen Phys. Rev. E 77, 051913 (2008)

•A 3D computational model that allow for changes in network geometry and account for their dynamic nature

•The model allow for the intersection points of polymers to move smoothly in three dimensions.

•The models describe a "cytoskeleton" in terms of randomly placed filaments linked together at their crossing points.



03-February-2010

Indian Institute of Technology Kanpur

J. Astrom, P.B. S. K., M. Karttunen and I. Vattulainen Phys. Rev. E 77, 051913 (2008)

•A 3D computational model that allow for changes in network geometry and account for their dynamic nature

- •The model allow for the intersection points of polymers to move smoothly in three dimensions.
- •The models describe a "cytoskeleton" in terms of randomly placed filaments linked together at their crossing points.
- •A full 3D mesh is obtained by depositing flexible filaments in a random fashion on a flat substrate.



03-February-2010

J. Astrom, P.B. S. K., M. Karttunen and I. Vattulainen Phys. Rev. E 77, 051913 (2008)

•A 3D computational model that allow for changes in network geometry and account for their dynamic nature

- •The model allow for the intersection points of polymers to move smoothly in three dimensions.
- •The models describe a "cytoskeleton" in terms of randomly placed filaments linked together at their crossing points.
- •A full 3D mesh is obtained by depositing flexible filaments in a random fashion on a flat substrate.
- A single fiber can be in contact with an arbitrary number of other fibers.



03-February-2010

Indian Institute of Technology Kanpur

J. Astrom, P.B. S. K., M. Karttunen and I. Vattulainen Phys. Rev. E 77, 051913 (2008)

•A 3D computational model that allow for changes in network geometry and account for their dynamic nature

- •The model allow for the intersection points of polymers to move smoothly in three dimensions.
- •The models describe a "cytoskeleton" in terms of randomly placed filaments linked together at their crossing points.
- •A full 3D mesh is obtained by depositing flexible filaments in a random fashion on a flat substrate.
- A single fiber can be in contact with an arbitrary number of other fibers.
- •The cross link between two fibers is described by a very short elastic element to allow for deformations to take place in a natural way.



03-February-2010

Indian Institute of Technology Kanpur

J. Astrom, P.B. S. K., M. Karttunen and I. Vattulainen Phys. Rev. E 77, 051913 (2008)

•A 3D computational model that allow for changes in network geometry and account for their dynamic nature

- •The model allow for the intersection points of polymers to move smoothly in three dimensions.
- •The models describe a "cytoskeleton" in terms of randomly placed filaments linked together at their crossing points.
- •A full 3D mesh is obtained by depositing flexible filaments in a random fashion on a flat substrate.
- A single fiber can be in contact with an arbitrary number of other fibers.
- •The cross link between two fibers is described by a very short elastic element to allow for deformations to take place in a natural way.





03-February-2010

Indian Institute of Technology Kanpur

J. Astrom, P.B. S. K., M. Karttunen and I. Vattulainen Phys. Rev. E 77, 051913 (2008)

•A 3D computational model that allow for changes in network geometry and account for their dynamic nature

- •The model allow for the intersection points of polymers to move smoothly in three dimensions.
- •The models describe a "cytoskeleton" in terms of randomly placed filaments linked together at their crossing points.
- •A full 3D mesh is obtained by depositing flexible filaments in a random fashion on a flat substrate.
- A single fiber can be in contact with an arbitrary number of other fibers.
- •The cross link between two fibers is described by a very short elastic element to allow for deformations to take place in a natural way.



Onck et. al PRL **95** 178102 (2005)



03-February-2010

Indian Institute of Technology Kanpur



The mesh obtained through this deposition process is taken as the (initial) equilibrium configuration.



03-February-2010

Indian Institute of Technology Kanpur



The mesh obtained through this deposition process is taken as the (initial) equilibrium configuration.

The mass of the fiber is modeled by a set of points (of equal mass "m") placed at equal distances along the fiber



03-February-2010

Indian Institute of Technology Kanpur



The mesh obtained through this deposition process is taken as the (initial) equilibrium configuration.

The mass of the fiber is modeled by a set of points (of equal mass "m") placed at equal distances along the fiber

The mass points of two different fibers, when they are closer than a threshold length are connected by a spring



03-February-2010

Indian Institute of Technology Kanpur



The mesh obtained through this deposition process is taken as the (initial) equilibrium configuration.

The mass of the fiber is modeled by a set of points (of equal mass "m") placed at equal distances along the fiber

The mass points of two different fibers, when they are closer than a threshold length are connected by a spring

Each fiber can be deformed either by stretching along its length or moving its end points perpendicular to its length



03-February-2010

Indian Institute of Technology Kanpur



The mesh obtained through this deposition process is taken as the (initial) equilibrium configuration.

The mass of the fiber is modeled by a set of points (of equal mass "m") placed at equal distances along the fiber

The mass points of two different fibers, when they are closer than a threshold length are connected by a spring

Each fiber can be deformed either by stretching along its length or moving its end points perpendicular to its length

Perpendicular deformations are predominantly bending.



03-February-2010

Indian Institute of Technology Kanpur

 $\mathbf{M}\ddot{\vec{r}} + \mathbf{C}\dot{\vec{r}} + \mathbf{K}\vec{r} = \vec{0}.$



03-February-2010

Indian Institute of Technology Kanpur





03-February-2010

Indian Institute of Technology Kanpur



The stiffness matrix *K* of the mesh is constructed by applying elastic interactions from the linear elastic beam theory to each of the straight fiber segments between two crossing points.(Euler-Bernoulli beam theory)



03-February-2010

Indian Institute of Technology Kanpur



The stiffness matrix *K* of the mesh is constructed by applying elastic interactions from the linear elastic beam theory to each of the straight fiber segments between two crossing points.(Euler-Bernoulli beam theory)

Global strain is applied by moving the two opposite boundaries in the x-direction by an amount $\,\delta x$.



03-February-2010

Indian Institute of Technology Kanpur



The stiffness matrix *K* of the mesh is constructed by applying elastic interactions from the linear elastic beam theory to each of the straight fiber segments between two crossing points.(Euler-Bernoulli beam theory)

Global strain is applied by moving the two opposite boundaries in the x-direction by an amount $\,\delta x$.

In constructing the stiffness matrix we take into account the stretching, bending, shearing, and torsional deformations of the filaments.



03-February-2010

Indian Institute of Technology Kanpur


M and *C* are diagonal matrices containing the mass and friction coefficient for each points

The stiffness matrix K of the mesh is constructed by applying elastic interactions from the linear elastic beam theory to each of the straight fiber segments between two crossing points.(Euler-Bernoulli beam theory)

Global strain is applied by moving the two opposite boundaries in the x-direction by an amount $\,\delta x$.

In constructing the stiffness matrix we take into account the stretching, bending, shearing, and torsional deformations of the filaments.

First we look at the case where all the cross links are fixed (Passive)



03-February-2010

Indian Institute of Technology Kanpur



M and *C* are diagonal matrices containing the mass and friction coefficient for each points

The stiffness matrix *K* of the mesh is constructed by applying elastic interactions from the linear elastic beam theory to each of the straight fiber segments between two crossing points.(Euler-Bernoulli beam theory)

Global strain is applied by moving the two opposite boundaries in the x-direction by an amount $\,\delta x$.

In constructing the stiffness matrix we take into account the stretching, bending, shearing, and torsional deformations of the filaments.

First we look at the case where all the cross links are fixed (Passive)







03-February-2010

Indian Institute of Technology Kanpur





03-February-2010

Indian Institute of Technology Kanpur



B.) The elastic energy of the fibers for the mesh as a function of strain



03-February-2010

Indian Institute of Technology Kanpur



B.) The elastic energy of the fibers for the mesh as a function of strain

C.) The second numerical derivative of the curve in Fig. B with respect to strain (Young's modulus of the mesh) as function of strain.



03-February-2010

Indian Institute of Technology Kanpur



B.) The elastic energy of the fibers for the mesh as a function of strain

C.) The second numerical derivative of the curve in Fig. B with respect to strain (Young's modulus of the mesh) as function of strain.

D.) Affine measure: The fraction of elastic energy of the fibers related to fiber stretching (as opposed to bending, stretching or torsion) as function of strain.



03-February-2010

Links are allowed to break when they are stretched beyond a threshold



03-February-2010

Indian Institute of Technology Kanpur

Links are allowed to break when they are stretched beyond a threshold





03-February-2010

Indian Institute of Technology Kanpur

Links are allowed to break when they are stretched beyond a threshold



A.) Snapshots of a mesh with semi-passive cross links at zero strain (left) and 100 % strain.

03-February-2010

Indian Institute of Technology Kanpur

Links are allowed to break when they are stretched beyond a threshold



A.) Snapshots of a mesh with semi-passive cross links at zero strain (left) and 100 % strain.

B.) The elastic energy of the fibers in mesh as a function of strain.Dotted line: curve from passive case for comparison.

03-February-2010

Indian Institute of Technology Kanpur

Links are allowed to break when they are stretched beyond a threshold



A.) Snapshots of a mesh with semi-passive cross links at zero strain (left) and 100 % strain.

B.) The elastic energy of the fibers in mesh as a function of strain.Dotted line: curve from passive case for comparison.

C.) The distribution of the strain at the links, between adjacent link fractures, for semi-passive links.



03-February-2010

Indian Institute of Technology Kanpur

Links are allowed to break when they are stretched beyond a threshold



A.) Snapshots of a mesh with semi-passive cross links at zero strain (left) and 100 % strain.

B.) The elastic energy of the fibers in mesh as a function of strain.Dotted line: curve from passive case for comparison.

C.) The distribution of the strain at the links, between adjacent link fractures, for semi-passive links.

D.) Elastic energy distribution of the links for small strain (i.e. before any link fractures). The distribution functions are approximately power-laws with 'cut-offs' at small and large strains. ^{03-February-2010} Indian Institute of Technology Kanpur

Comparison with experiments

Below the transition, the elastic energy (Ee) has a weak dependence on r and above the critical value it varies as $(r - r_c)^{1.5}$





Plateau modulus G_0 as a function of the molar ratio R of fascin with respect to actin for two different concentrations of actin: 0.4 mg/ml (circles) and 0.2 mg/ml (squares).

O. Lieleg et. al. Phys. Rev. Lett., 99, 088102 (2007).

03-February-2010

Indian Institute of Technology Kanpur

Comparison with experiments

Below the transition, the elastic energy (Ee) has a weak dependence on r and above the critical value it varies as $(r - r_c)^{1.5}$



J. Astrom, P.B. S. K., M. Karttunen and I. Vattulainen Phys. Rev. E 77, 051913 (2008)



Plateau modulus G_0 as a function of the molar ratio R of fascin with respect to actin for two different concentrations of actin: 0.4 mg/ml (circles) and 0.2 mg/ml (squares).

O. Lieleg et. al. Phys. Rev. Lett., 99, 088102 (2007).

03-February-2010

Indian Institute of Technology Kanpur





Differential modulus K versus deformation for fascin networks in the bundle phase and increasing R. The inset shows the critical strain in dependence on R.

O. Lieleg et. al. Phys. Rev. Lett., 99, 088102 (2007).



03-February-2010

Indian Institute of Technology Kanpur



 $\left[\begin{array}{c} \mathbf{r} \\ \mathbf{r} \\$

Differential modulus K versus deformation for fascin networks in the bundle phase and increasing R. The inset shows the critical strain in dependence on R.

O. Lieleg et. al. Phys. Rev. Lett., 99, 088102 (2007).



03-February-2010

Indian Institute of Technology Kanpur

Links can break and form as the fibers move away and close to each other



03-February-2010

Indian Institute of Technology Kanpur

Links can break and form as the fibers move away and close to each other



03-February-2010

Indian Institute of Technology Kanpur

Links can break and form as the fibers move away and close to each other



A.) Snapshots of a mesh with active cross links at different strains. The first three snapshots are prior to the stress maximum while the last is after maximum strain is reached.

03-February-2010

Indian Institute of Technology Kanpur

Links can break and form as the fibers move away and close to each other



A.) Snapshots of a mesh with active cross links at different strains. The first three snapshots are prior to the stress maximum while the last is after maximum strain is reached.

B.) The elastic energy of the fibers for the mesh in (A) as function of strain (full line).Dashed line: curve from passive model for comparison.



03-February-2010

Indian Institute of Technology Kanpur

Links can break and form as the fibers move away and close to each other



A.) Snapshots of a mesh with active cross links at different strains. The first three snapshots are prior to the stress maximum while the last is after maximum strain is reached.

B.) The elastic energy of the fibers for the mesh in (A) as function of strain (full line).Dashed line: curve from passive model for comparison.

C.) The number of cross links as function of strain..



03-February-2010

Indian Institute of Technology Kanpur



Stretch induced stress fiber formation in cells in Bovine aortic endothelial cells. Cells were stained with rhodamine-phalloidin to identify f-actin bundles

R. Kaunas, P. Nguyen, S. Usami, and S.Chien, PNAS 102, 15895 ((2005)



03-February-2010

Indian Institute of Technology Kanpur



03-February-2010

Indian Institute of Technology Kanpur

In vitro experiments are mostly with stabilized microtubules



03-February-2010

Indian Institute of Technology Kanpur

In vitro experiments are mostly with stabilized microtubules



Thomas Surrey, et al. Science , 1167 (2001); 292



03-February-2010

Indian Institute of Technology Kanpur

In vitro experiments are mostly with stabilized microtubules



Thomas Surrey, et al. Science , 1167 (2001); 292



03-February-2010

Indian Institute of Technology Kanpur





In vitro experiments are mostly with stabilized microtubules

A First binding Pon Pon Poff Poff Diffusion Poff,end Poff,end Poff,end Poff,end Poff,end

03-February-2010

Indian Institute of Technology Kanpur



In vitro experiments are mostly with stabilized microtubules

Thomas Surrey, et al. Science , 1167 (2001); 292



•Many parameters: Not clear which are important

•No elasticity



high motor density

03-February-2010

Indian Institute of Technology Kanpur



In vitro experiments are mostly with stabilized microtubules



•Many parameters: Not clear which are important

•No elasticity

S.Sankararaman, G. Menon, P.B.S.K. Phys. Rev. E. 70, 031905 (2004) - a hydrodynamic model

03-February-2010

Indian Institute of Technology Kanpur



03-February-2010

Indian Institute of Technology Kanpur





03-February-2010

Indian Institute of Technology Kanpur



•3D elastic network

- •Motor cross-linkers move along the fibers
- •Motors may get strained as they move
- •Threshold strain for stalling τ_c
- -Threshold strain for detaching $\,\tau_{\text{b}}$



03-February-2010

Indian Institute of Technology Kanpur



•3D elastic network

- •Motor cross-linkers move along the fibers
- •Motors may get strained as they move
- •Threshold strain for stalling $~~\tau_c$
- -Threshold strain for detaching $\,\tau_{\text{b}}$



(A.) 500 Randomly placed filaments with free boundary condition.

(B) When motors are unidirectional asters form

(C) Stead state configuration with bidirectional motors.



03-February-2010

Indian Institute of Technology Kanpur



•3D elastic network

- •Motor cross-linkers move along the fibers
- •Motors may get strained as they move
- •Threshold strain for stalling $~~\tau_{c}$
- -Threshold strain for detaching $\,\tau_{\text{b}}$



(A.) 500 Randomly placed filaments with free boundary condition.

(B) When motors are unidirectional asters form

(C) Stead state configuration with bidirectional motors.

J. Astrom, P. B. S. K. and M. Karttunen: Soft Matter , **5**, 2869 (2009) Elastic energy as a function of time



03-February-2010



The elastic energy stored in the motors E_{cl} as function of time for $\tau_b = 0.2, 0.3, ..., 0.7$ (yellow, green, blue, red, magenta, black) with $\tau_c = 0.3$



(A) Initial configuration with clamped boundary. The mesh contains 1000 fibers. Its size 4.2 X 4.2 X 1. $T_c = 0.2$ (B) Final steady state configuration for $T_b=0.3$ (C)Final steady state configuration for $T_b=0.6$



03-February-2010

Indian Institute of Technology Kanpur


The elastic energy stored in the motors E_{cl} as function of time for $\tau_b = 0.2, 0.3, ..., 0.7$ (yellow, green, blue, red, magenta, black) with $\tau_c = 0.3$



(A) Initial configuration with clamped boundary. The mesh contains 1000 fibers. Its size 4.2 X 4.2 X 1. $T_c = 0.2$ (B) Final steady state configuration for $T_b=0.3$ (C)Final steady state configuration for $T_b=0.6$

J. Astrom, P. B. S. K. and M. Karttunen: Soft Matter, 5, 2869 (2009)



03-February-2010

Indian Institute of Technology Kanpur



The ratio of the steady to the maximum value of elastic energy as a function of τ_b and τ_b/τ_c for different values of τ_b and τ_c for clamped (A,B,D) and free boundaries (C). Symbols are for different parameter values. The critical $\tau b/\tau c$ seems to agree with experiments (see Nature **377**,251 (1995) , Nature 368, **113**, 1994)

03-February-2010

Indian Institute of Technology Kanpur



03-February-2010

Indian Institute of Technology Kanpur

• A 3D elastic network model, that allows for changes in the network geometry in response to an externally imposed strain, is discussed. This model represents a network of actin filaments which has the ability, as real cytoskeletal networks do, to adjust its cross links dynamically.



03-February-2010

Indian Institute of Technology Kanpur

- A 3D elastic network model, that allows for changes in the network geometry in response to an externally imposed strain, is discussed. This model represents a network of actin filaments which has the ability, as real cytoskeletal networks do, to adjust its cross links dynamically.
- This stiff elastic rod model will be applicable in the regime corresponding to dense actin networks, as in the case of the cytoskeleton.



03-February-2010

Indian Institute of Technology Kanpur

- A 3D elastic network model, that allows for changes in the network geometry in response to an externally imposed strain, is discussed. This model represents a network of actin filaments which has the ability, as real cytoskeletal networks do, to adjust its cross links dynamically.
- This stiff elastic rod model will be applicable in the regime corresponding to dense actin networks, as in the case of the cytoskeleton.
- We have found strain hardening without entropic elasticity.



03-February-2010

Indian Institute of Technology Kanpur

- A 3D elastic network model, that allows for changes in the network geometry in response to an externally imposed strain, is discussed. This model represents a network of actin filaments which has the ability, as real cytoskeletal networks do, to adjust its cross links dynamically.
- This stiff elastic rod model will be applicable in the regime corresponding to dense actin networks, as in the case of the cytoskeleton.
- We have found strain hardening without entropic elasticity.
- We have shown that the strain hardening in these dense networks is due to a change from a bending dominated regime to the stretching dominated one.



03-February-2010

Indian Institute of Technology Kanpur

- A 3D elastic network model, that allows for changes in the network geometry in response to an externally imposed strain, is discussed. This model represents a network of actin filaments which has the ability, as real cytoskeletal networks do, to adjust its cross links dynamically.
- This stiff elastic rod model will be applicable in the regime corresponding to dense actin networks, as in the case of the cytoskeleton.
- We have found strain hardening without entropic elasticity.
- We have shown that the strain hardening in these dense networks is due to a change from a bending dominated regime to the stretching dominated one.
- An active model of cross linkers, with links breaking and forming, shows structures similar to stress fibers.



03-February-2010

Indian Institute of Technology Kanpur

- A 3D elastic network model, that allows for changes in the network geometry in response to an externally imposed strain, is discussed. This model represents a network of actin filaments which has the ability, as real cytoskeletal networks do, to adjust its cross links dynamically.
- This stiff elastic rod model will be applicable in the regime corresponding to dense actin networks, as in the case of the cytoskeleton.
- We have found strain hardening without entropic elasticity.
- We have shown that the strain hardening in these dense networks is due to a change from a bending dominated regime to the stretching dominated one.
- An active model of cross linkers, with links breaking and forming, shows structures similar to stress fibers.
- The results from the semi-passive simulations seems to be in good agreement with recent experiments.



03-February-2010

Indian Institute of Technology Kanpur

- A 3D elastic network model, that allows for changes in the network geometry in response to an externally imposed strain, is discussed. This model represents a network of actin filaments which has the ability, as real cytoskeletal networks do, to adjust its cross links dynamically.
- This stiff elastic rod model will be applicable in the regime corresponding to dense actin networks, as in the case of the cytoskeleton.
- We have found strain hardening without entropic elasticity.
- We have shown that the strain hardening in these dense networks is due to a change from a bending dominated regime to the stretching dominated one.
- An active model of cross linkers, with links breaking and forming, shows structures similar to stress fibers.
- The results from the semi-passive simulations seems to be in good agreement with recent experiments.
- Pattern formation in a system of fully mobile cross linkers and elastic filaments, with surface anchoring, is studied.



03-February-2010

Indian Institute of Technology Kanpur

- A 3D elastic network model, that allows for changes in the network geometry in response to an externally imposed strain, is discussed. This model represents a network of actin filaments which has the ability, as real cytoskeletal networks do, to adjust its cross links dynamically.
- This stiff elastic rod model will be applicable in the regime corresponding to dense actin networks, as in the case of the cytoskeleton.
- We have found strain hardening without entropic elasticity.
- We have shown that the strain hardening in these dense networks is due to a change from a bending dominated regime to the stretching dominated one.
- An active model of cross linkers, with links breaking and forming, shows structures similar to stress fibers.
- The results from the semi-passive simulations seems to be in good agreement with recent experiments.
- Pattern formation in a system of fully mobile cross linkers and elastic filaments, with surface anchoring, is studied.
- we demonstrate that, for unidirectional motors, two basic contractile phases emerge in these systems. The transition is governed by a single parameter (τ_b / τ_c)



03-February-2010

Indian Institute of Technology Kanpur

- A 3D elastic network model, that allows for changes in the network geometry in response to an externally imposed strain, is discussed. This model represents a network of actin filaments which has the ability, as real cytoskeletal networks do, to adjust its cross links dynamically.
- This stiff elastic rod model will be applicable in the regime corresponding to dense actin networks, as in the case of the cytoskeleton.
- We have found strain hardening without entropic elasticity.
- We have shown that the strain hardening in these dense networks is due to a change from a bending dominated regime to the stretching dominated one.
- An active model of cross linkers, with links breaking and forming, shows structures similar to stress fibers.
- The results from the semi-passive simulations seems to be in good agreement with recent experiments.
- Pattern formation in a system of fully mobile cross linkers and elastic filaments, with surface anchoring, is studied.
- we demonstrate that, for unidirectional motors, two basic contractile phases emerge in these systems. The transition is governed by a single parameter (τ_b / τ_c)
- The link between structure and elasticity is further probed through a bidirectional network.



03-February-2010

Indian Institute of Technology Kanpur

- A 3D elastic network model, that allows for changes in the network geometry in response to an externally imposed strain, is discussed. This model represents a network of actin filaments which has the ability, as real cytoskeletal networks do, to adjust its cross links dynamically.
- This stiff elastic rod model will be applicable in the regime corresponding to dense actin networks, as in the case of the cytoskeleton.
- We have found strain hardening without entropic elasticity.
- We have shown that the strain hardening in these dense networks is due to a change from a bending dominated regime to the stretching dominated one.
- An active model of cross linkers, with links breaking and forming, shows structures similar to stress fibers.
- The results from the semi-passive simulations seems to be in good agreement with recent experiments.
- Pattern formation in a system of fully mobile cross linkers and elastic filaments, with surface anchoring, is studied.
- we demonstrate that, for unidirectional motors, two basic contractile phases emerge in these systems. The transition is governed by a single parameter (τ_b / τ_c)
- The link between structure and elasticity is further probed through a bidirectional network.
- We show that a stiffness transition takes place, about the percolation transition, as the number of parallel filaments are varied.

03-February-2010

Indian Institute of Technology Kanpur



Jan





Jan Astrom - CSC, Finnish IT Center for Science Helsinki , Finland Ilpo Vattulainen - Tampere University of Technology, Finland Mikko Karttunen- The University of Western Ontario, London, Ontario, Canada Computational resources - University of Southern Denmark, CSC - Finland, HPCE- IIT Madras .



03-February-2010

Indian Institute of Technology Kanpur

Wednesday 10 February 2010

Mikko

llpo